

WIR SCHAFFEN WISSEN - HEUTE FÜR MORGEN



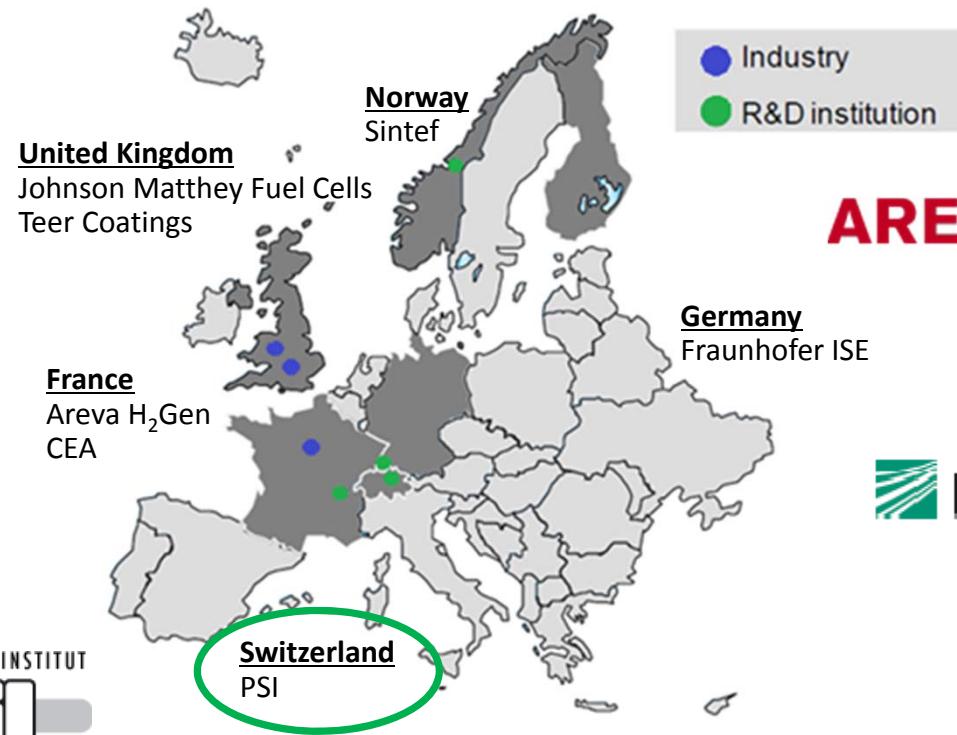
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Membranes for Water Electrolysis - Target-Oriented Choice and Design of Materials

Durability and Degradation Issues in PEM Electrolysis Cells and its Components

February 16, 2016 :: Fraunhofer ISE, Freiburg, Germany

Acknowledgement



AREVA H₂Gen

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- Loss terms in PEM electrolysis

Selection Criteria for Membranes

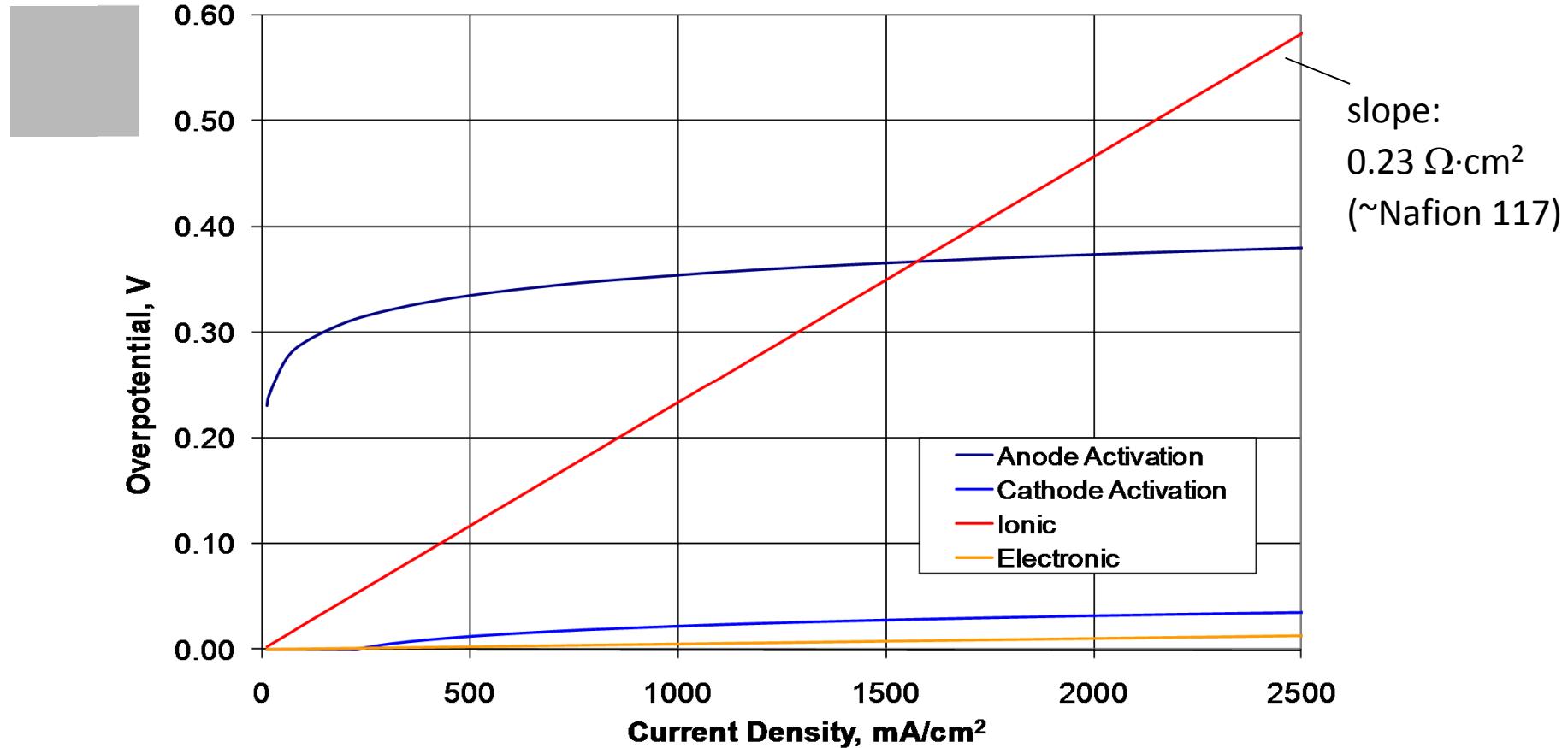
- A simple performance model
- Resistance - gas crossover tradeoff
- Membrane development within NOVEL

Durability Aspects

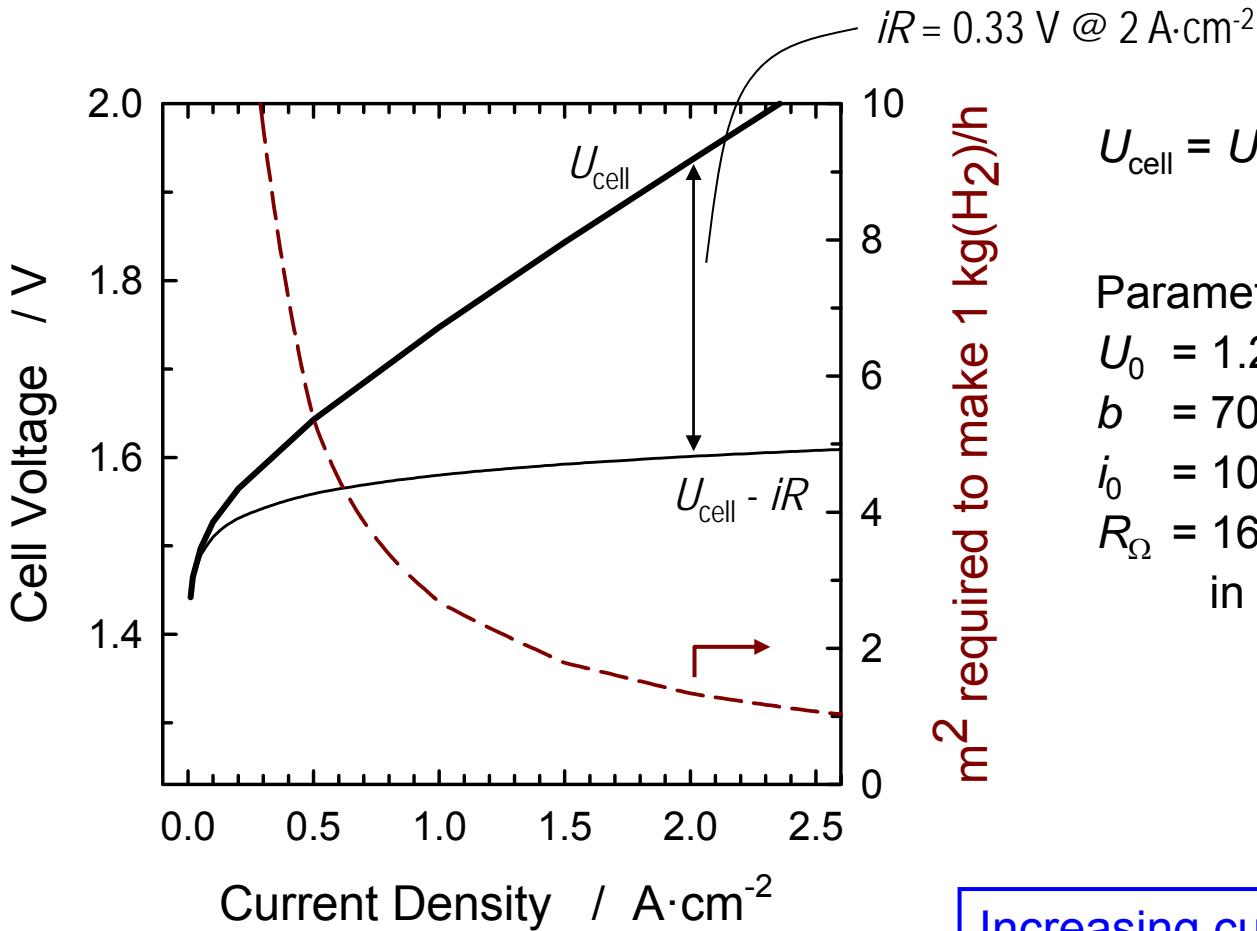
- Radical-induced degradation
- Thermal stress test

Conclusion

Loss Terms in PEM Electrolysis



Simple Electrolysis Model



$$U_{cell} = U_0 + b \cdot \log(i/i_0) + iR_\Omega :$$

Parameters:

$$U_0 = 1.23 \text{ V}$$

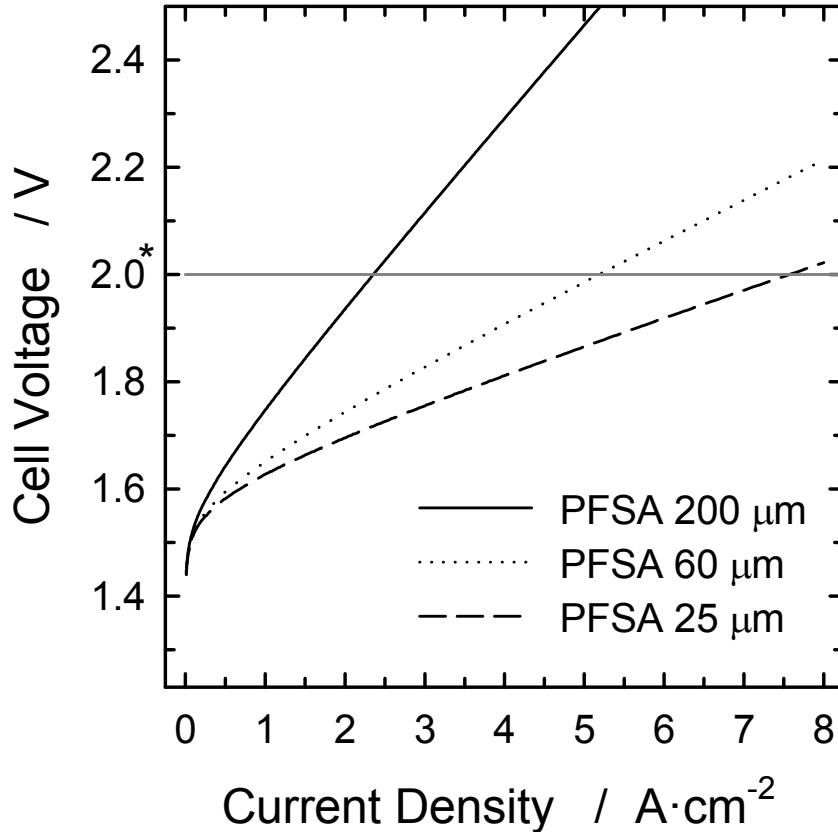
$$b = 70 \text{ mV/decade}$$

$$i_0 = 10^{-5} \text{ A/cm}^2_{geom}$$

$$R_\Omega = 167 \Omega \cdot \text{cm}^2 \text{ (Nafion 117 in water @ } 80^\circ\text{C)}$$

Increasing current density can reduce size of electrolyzer

Reducing Membrane Thickness



* $\eta = 74\% \text{ (HHV)}$

$$R_\Omega = R_0 + R_m$$

non-membrane ohmic resistance:

$$R_0 \approx 30 \text{ m}\Omega \cdot \text{cm}^2$$

$$R_m = \delta / \sigma$$

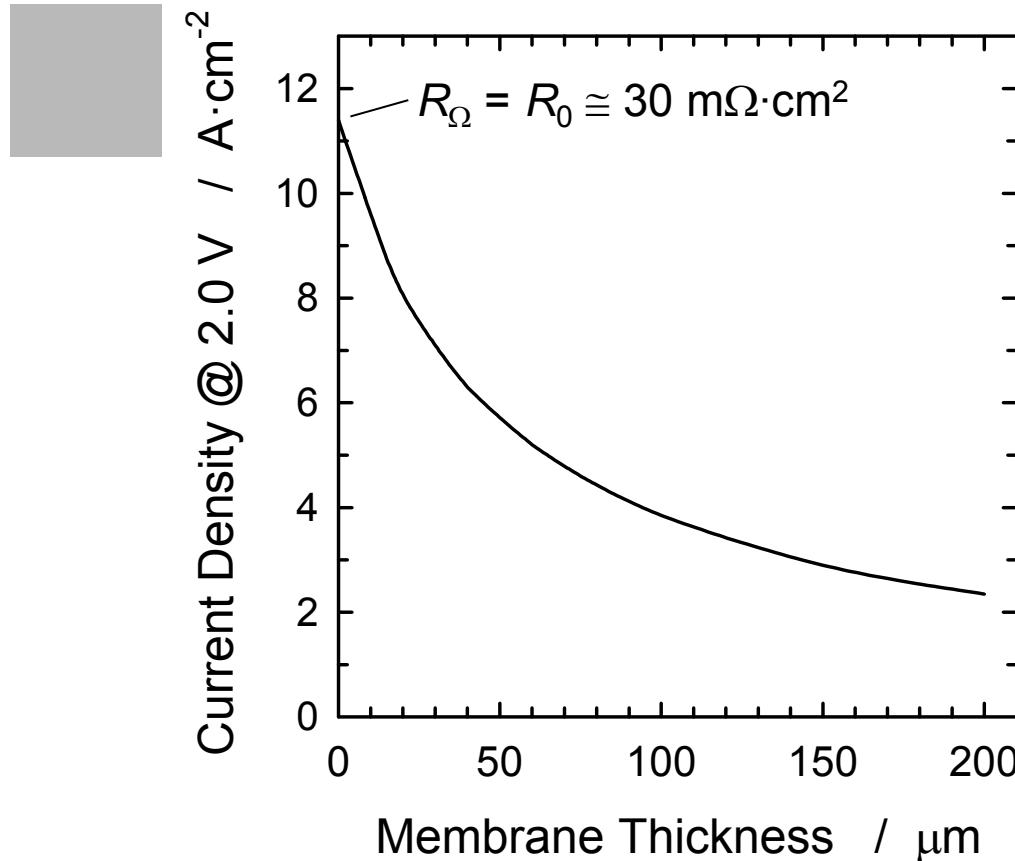
conductivity

membrane thickness

| δ (μm) | R_Ω ($\text{m}\Omega \cdot \text{cm}^2$) |
|----------------------------|---|
| 200 | 167 |
| 60 | 71 |
| 25 | 47 |

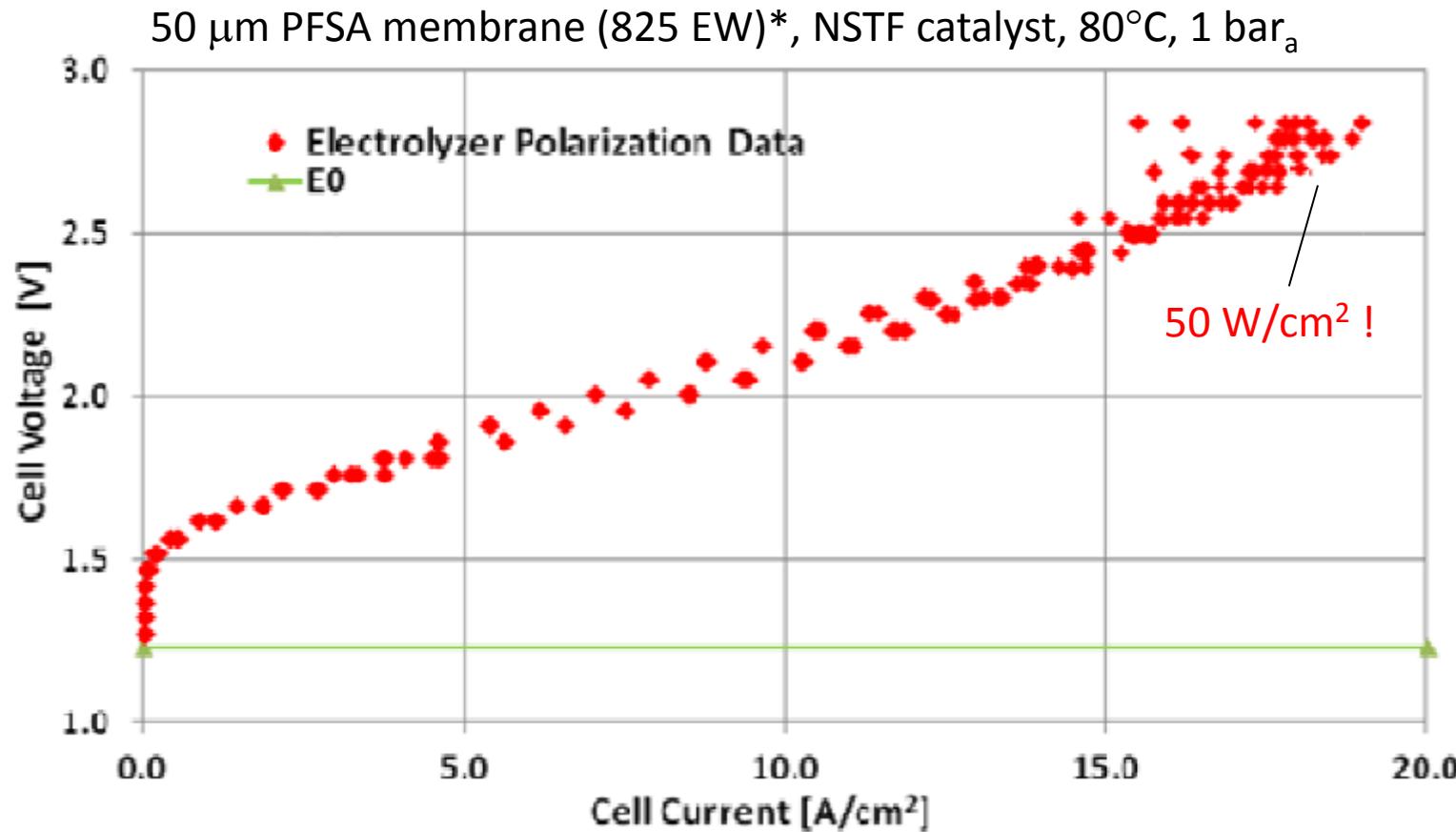
Reducing membrane thickness allows much higher current density at given cell voltage (i.e., efficiency)

Reducing Membrane Thickness



Residual ohmic resistance R_0 may increase over time due to passivation of Ti current collector and bipolar plate

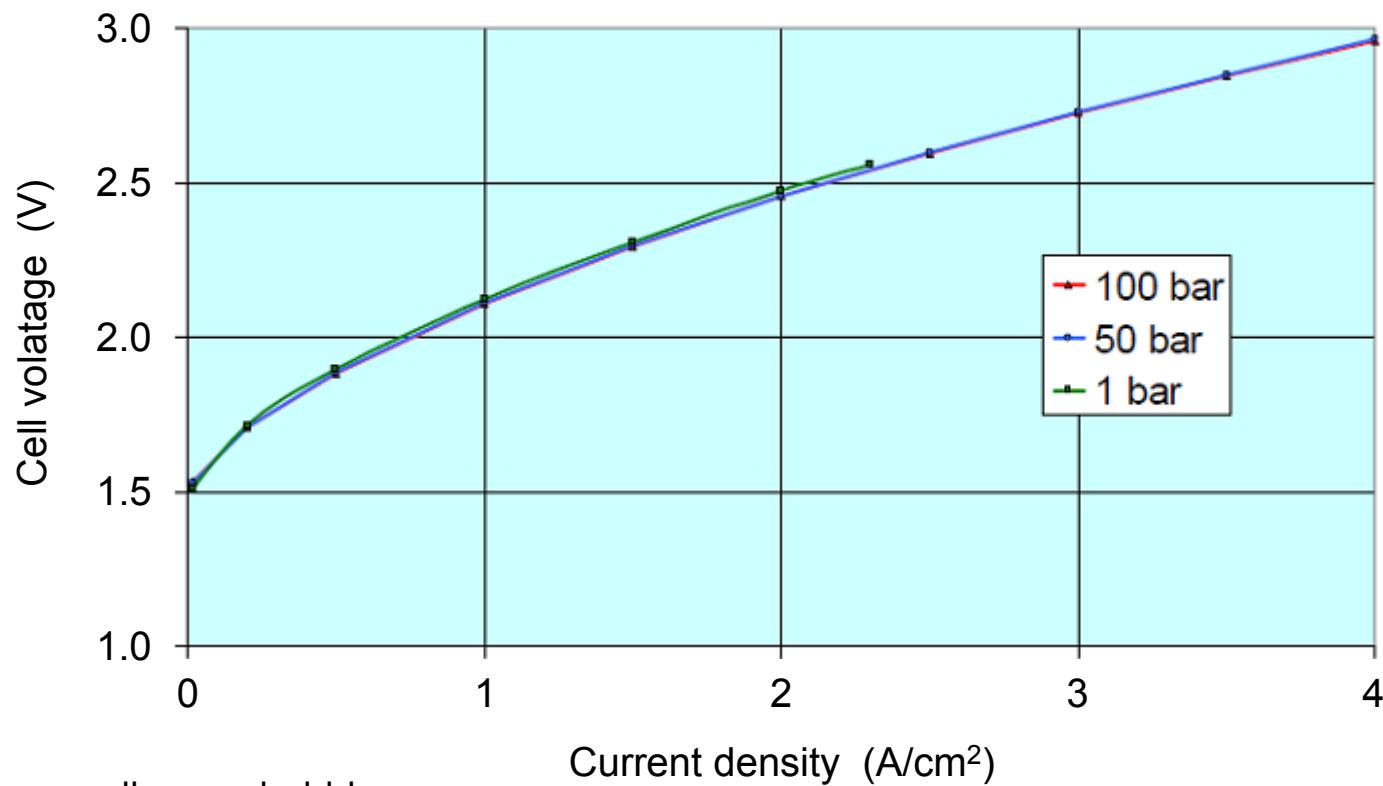
Performance reported by 3M



* $\sigma \approx 0.25 \text{ S}/\text{cm} @ 80^\circ\text{C}$

Thermal management ?

High Pressure Operation: Lab Test Data

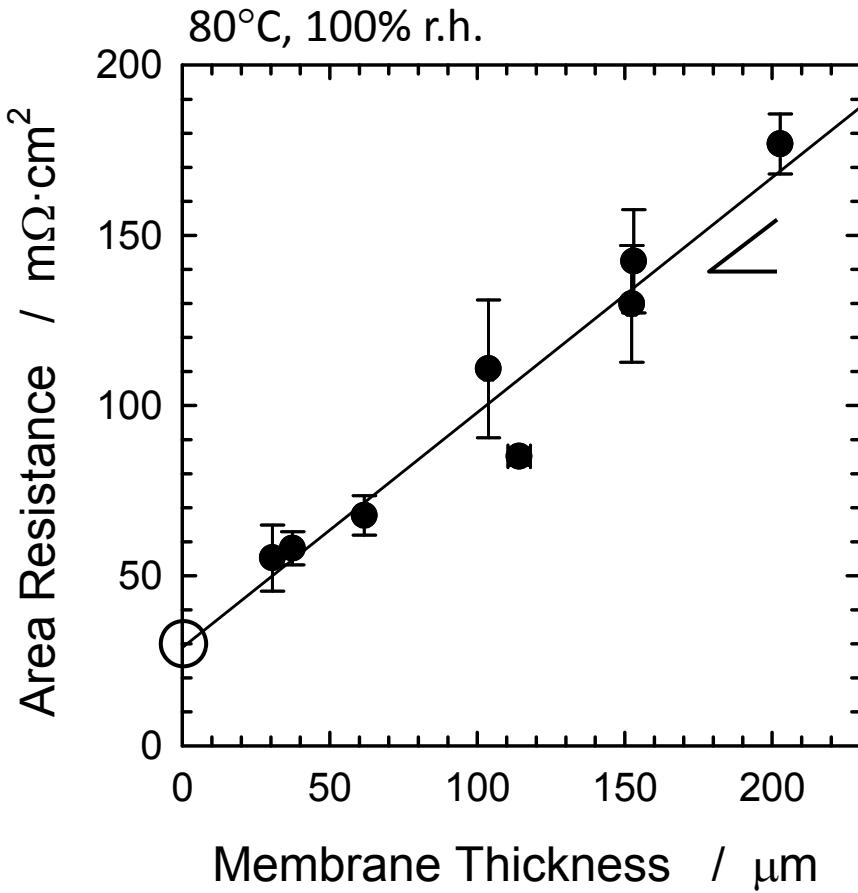


$p \uparrow \rightarrow$ smaller gas bubbles
 \rightarrow lower mass transport losses

A. Reiner, Siemens

There is little influence of the pressure on the polarization behavior of the electrolysis cell

Area Resistance and Membrane Thickness



Area resistance R_Ω
 (Nafion with EW 1'100):

$$R_\Omega = R_0 + R_m$$

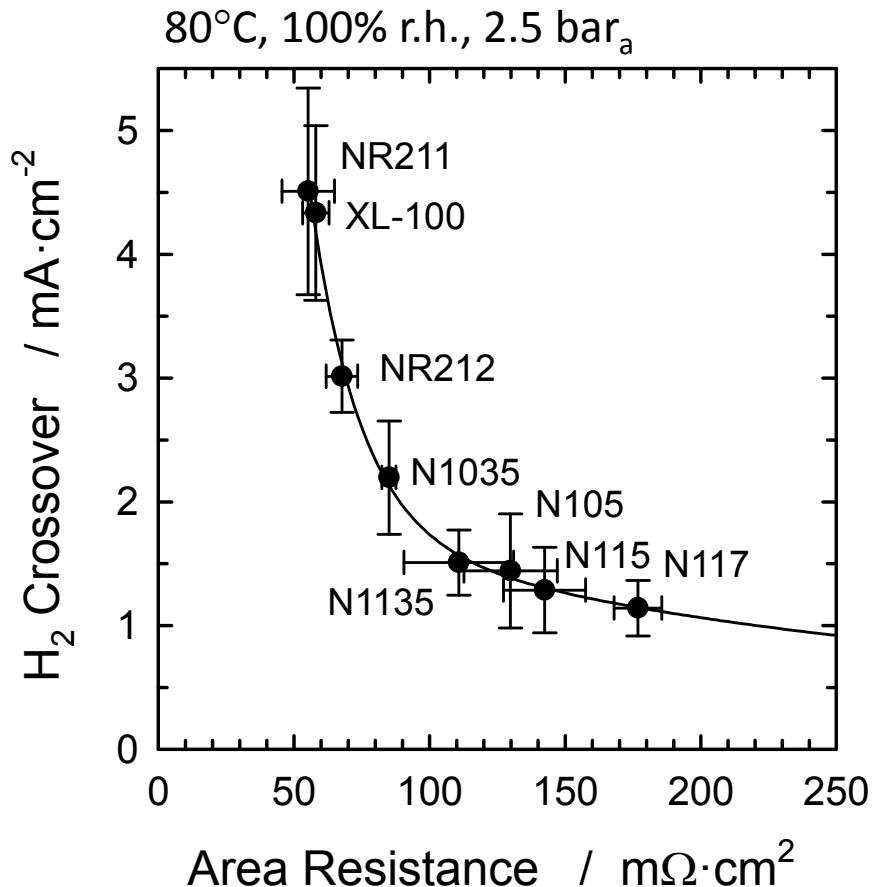
$$R_m = \delta / \sigma$$

fitting parameters:

$$R_0 = 30 \Omega\cdot\text{cm}^2$$

$$\sigma = 146 \text{ mS/cm}$$

Resistance - Gas Crossover Tradeoff



fit H₂ crossover i_x :

$$i_x = 2F \frac{P(H_2)}{\delta} p$$

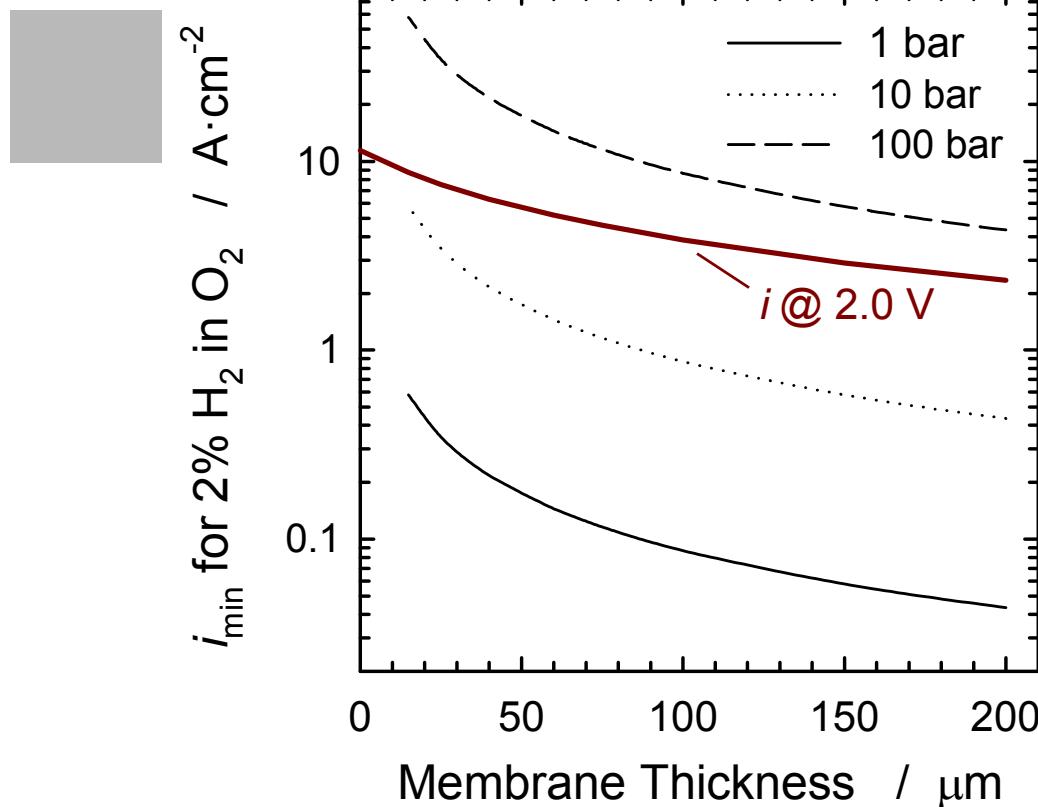
$$\rightarrow P(H_2) = 4.5 \cdot 10^{-13} \frac{\text{mol} \cdot \text{cm}}{\text{cm}^2 \cdot \text{s} \cdot \text{kPa}}$$

fit area resistance R_Ω (EW 1'100):

$$R_\Omega = R_0 + \delta / \sigma$$

$$\rightarrow R_0 = 30 \Omega \cdot \text{cm}^2, \sigma = 146 \text{ mS/cm}$$

Gas Crossover - Minimum Current Density



Nafion gas permeabilities

| $P(\text{H}_2)$ mol·cm cm ² ·s·kPa | $P(\text{O}_2)$ mol·cm cm ² ·s·kPa | Ref. |
|---|---|------|
| $5.32 \cdot 10^{-13}$ | $2.52 \cdot 10^{-13}$ | 1 |
| $5.10 \cdot 10^{-13}$ | $2.70 \cdot 10^{-13}$ | 2 |
| $1.8 \cdot 10^{-13}$ | $8.0 \cdot 10^{-14}$ | 3 |
| $4.50 \cdot 10^{-13}$ | n/a | 4 |

$$P(\text{H}_2) \approx 2 \times P(\text{O}_2)$$

$$c(\text{O}_2 \text{ in H}_2) = p \cdot \frac{P(\text{O}_2)}{\delta} \cdot \frac{2F}{i}$$

$$\begin{aligned} c(\text{H}_2 \text{ in O}_2) &= p \cdot \frac{P(\text{H}_2)}{\delta} \cdot \frac{4F}{i} \\ &\approx 4 \times c(\text{O}_2 \text{ in H}_2) \end{aligned}$$

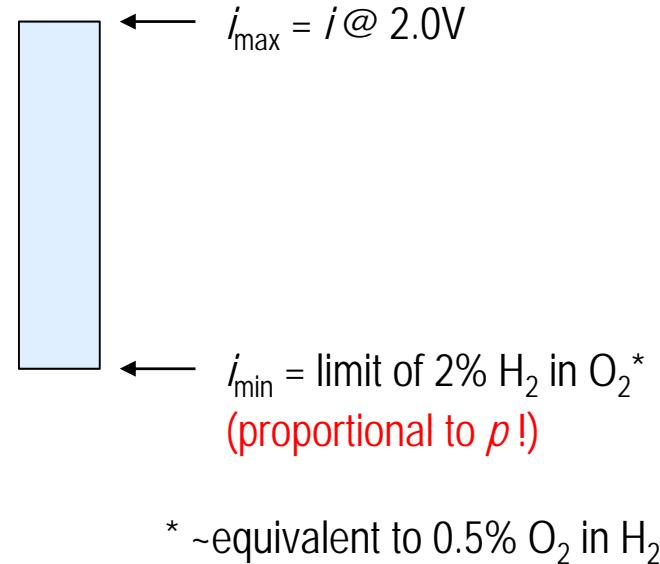
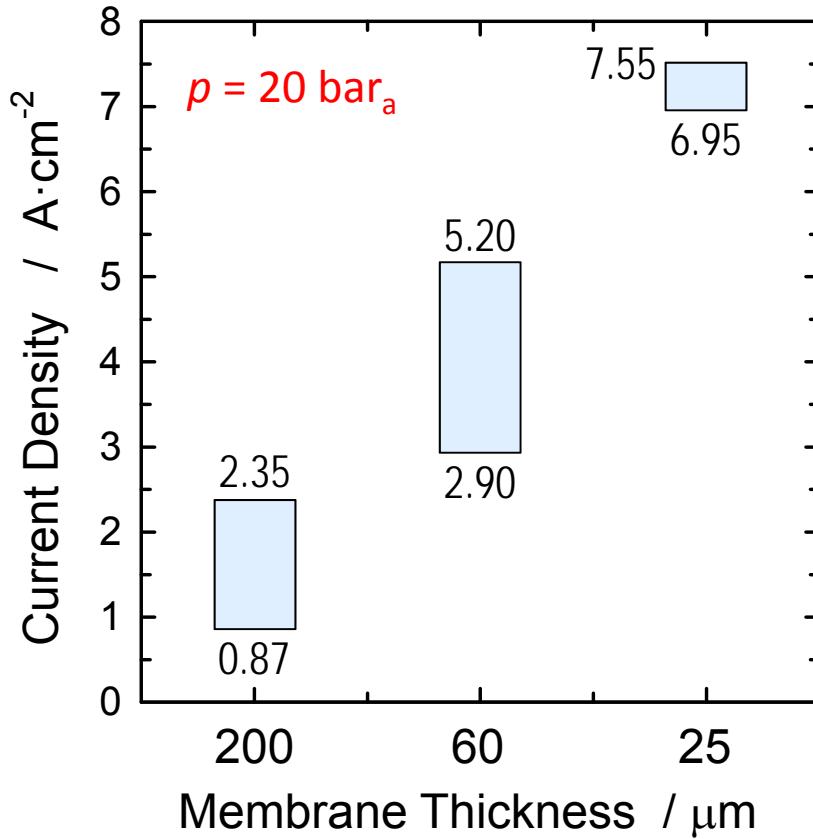
¹ M. Schalenbach et al., *J. Phys. Chem. C* **119** (2015) 25145

² T. Sakai et al., *J. Electrochem. Soc.* **132** (1985) 1328

³ Z. Zhang et al., *J. Membr. Sci.* **472** (2014) 55

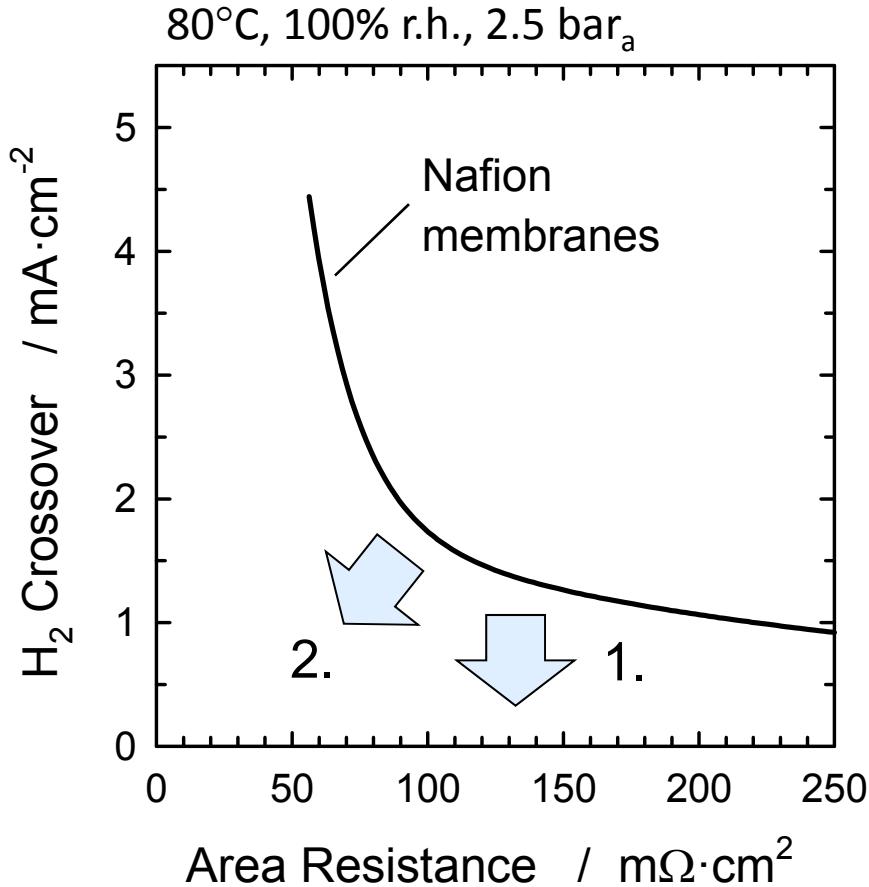
⁴ fit of H₂ crossover data

Operational Range (Turndown Ratio)



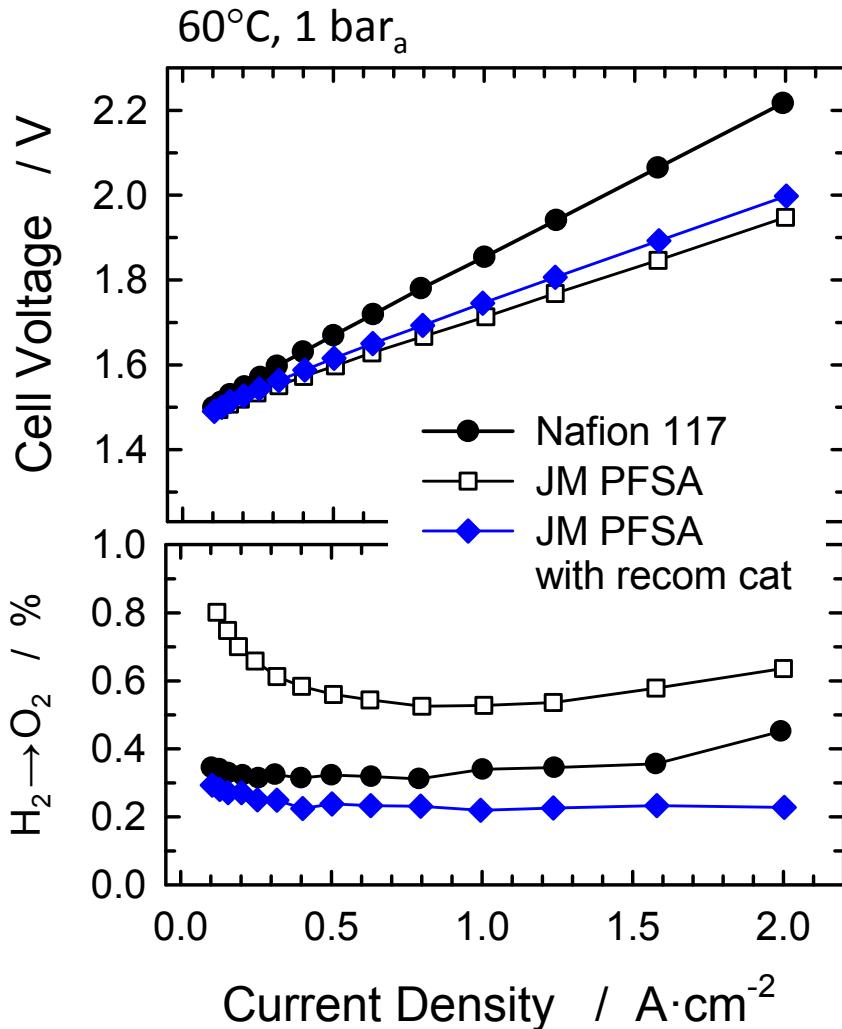
Operational range with thin membranes is limited due to crossover issue
 → Need to increase gas barrier properties of membrane

Membrane Development Strategies



- 1. PFSA membranes**
improve gas barrier properties
- 2. Alternative membranes**
choose materials with intrinsically better combination of resistance and gas permeability

Reinforced PFSA Membranes with Recombination Catalyst



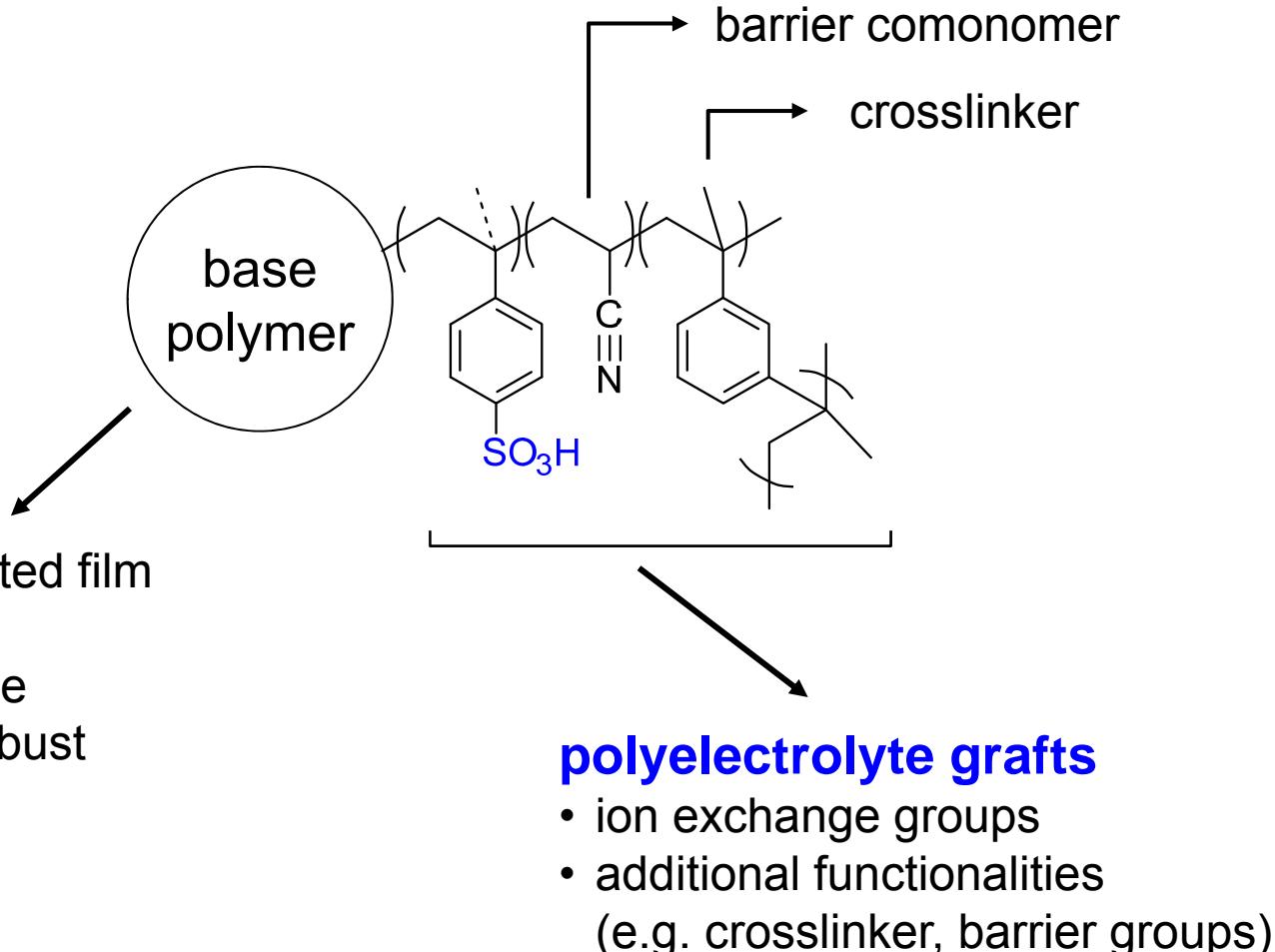
JM PFSA membrane:
 (adapted automotive membrane)

- thickness ~60 µm
- reinforced
- containing PGM-type H₂-O₂ **recombination catalyst**

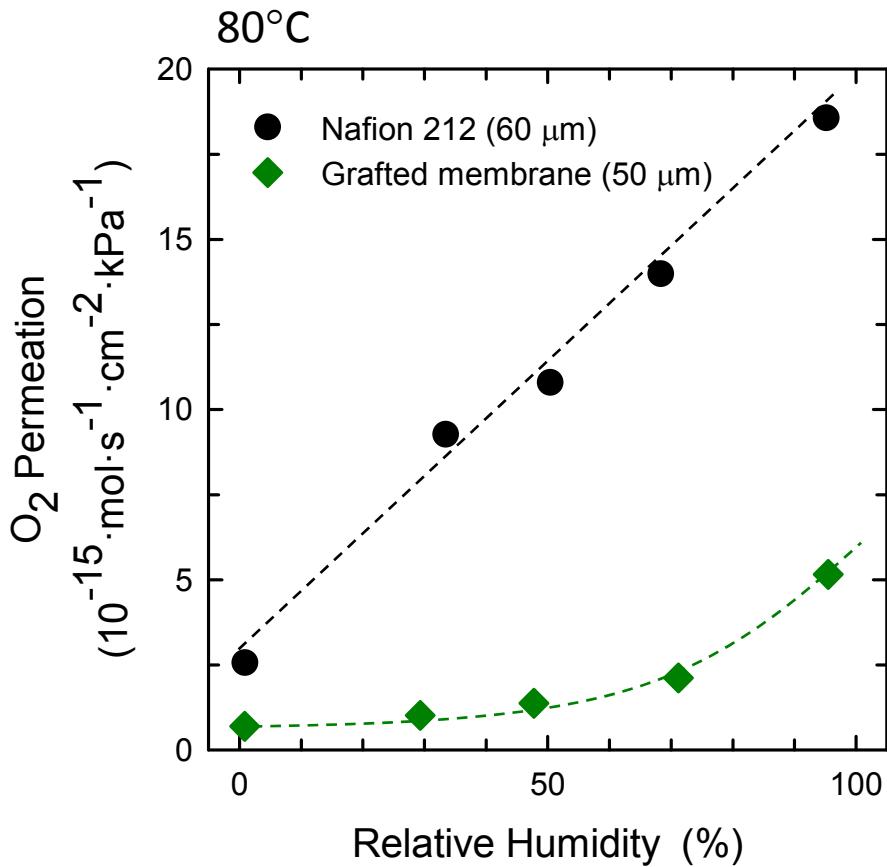
- Improved performance
- lower gas crossover

Ion Conducting Graft Copolymer Membranes

- partially fluorinated film (ETFE, ECTFE)
- chemically stable
- mechanically robust



Gas Permeation Properties

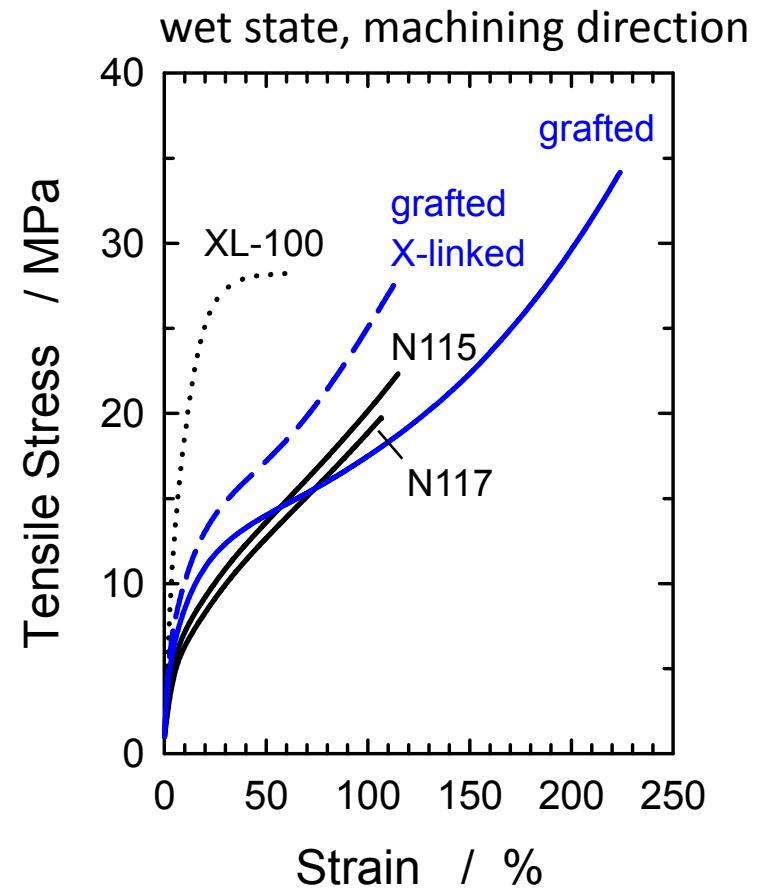
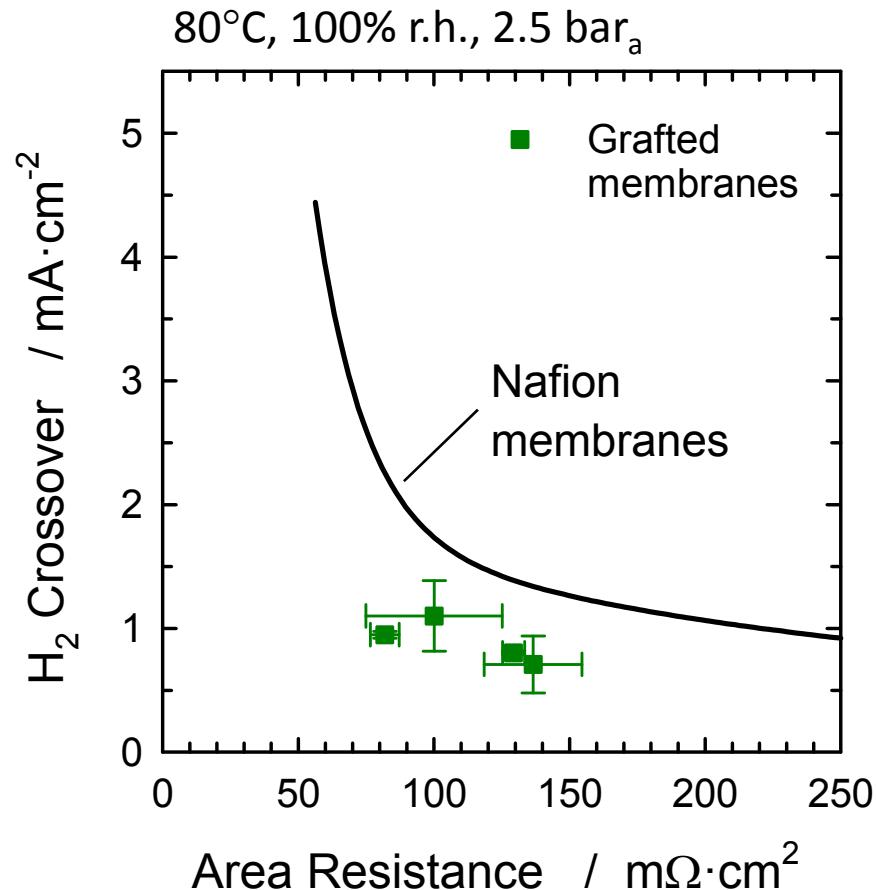


Gas permeation measured
by mass spectrometry method*

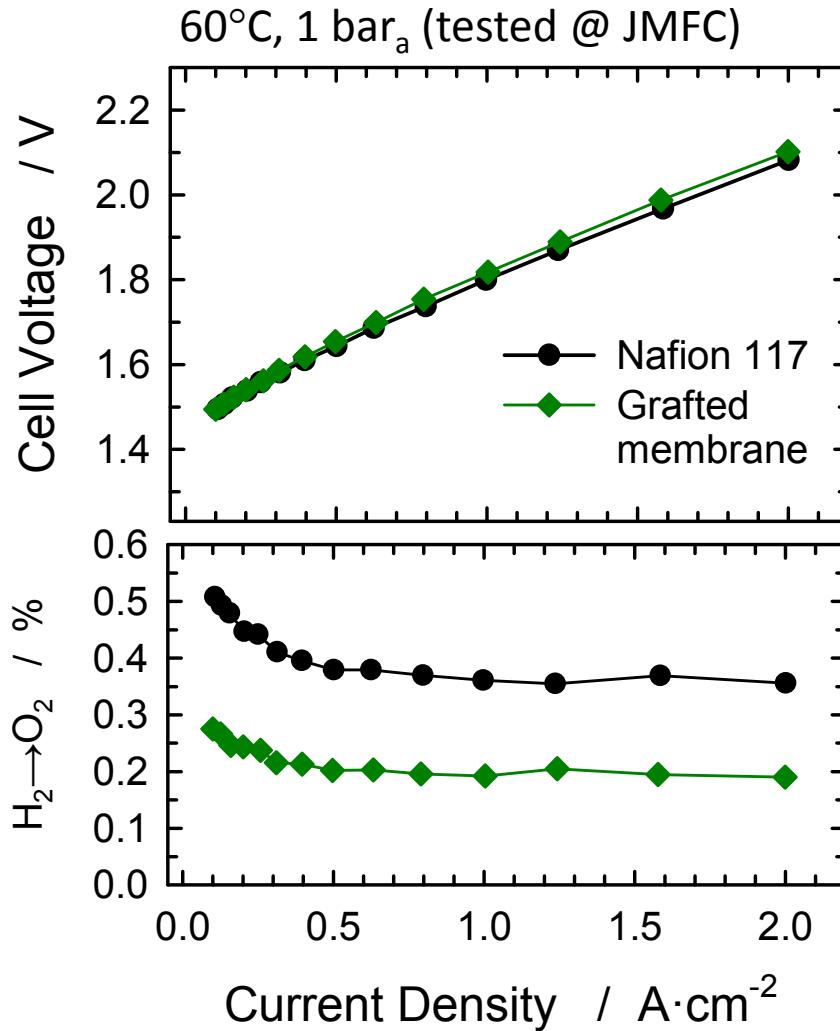
Grafted membrane shows
much lower gas crossover

* Z. Zhang et al., *J. Membr. Sci.* **472** (2014) 55

Property Map



Cell Performance with Grafted Membrane

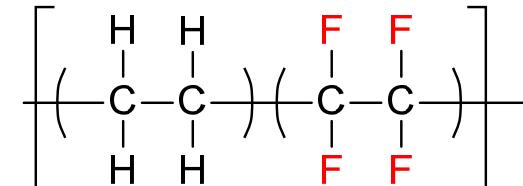
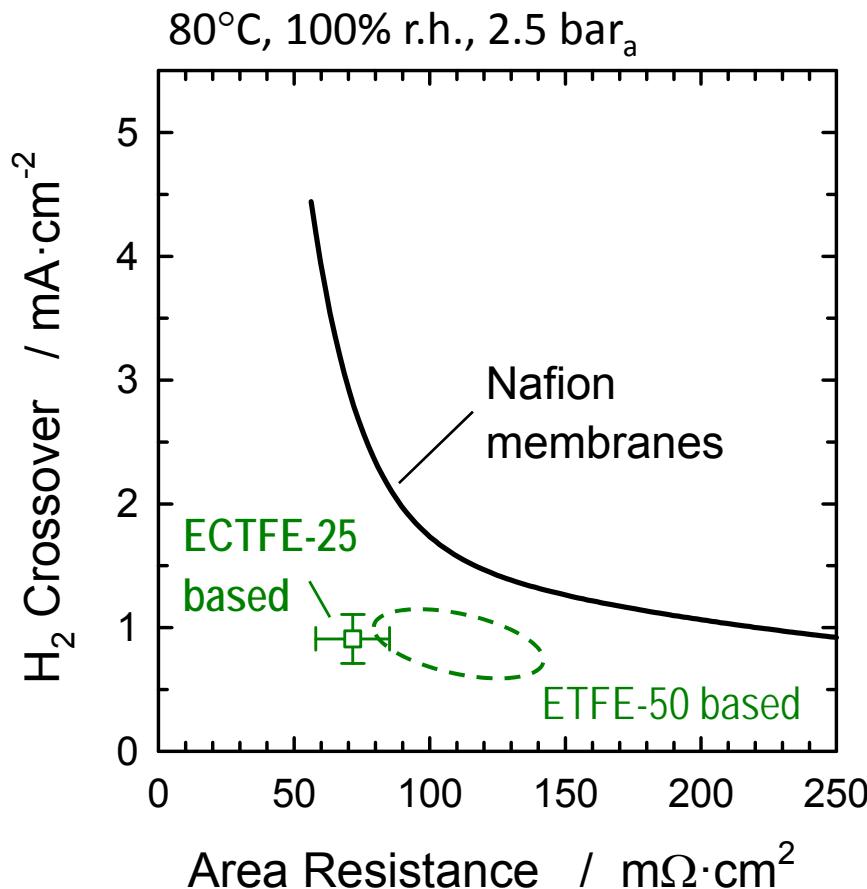


Grafted membrane vs. Nafion 117

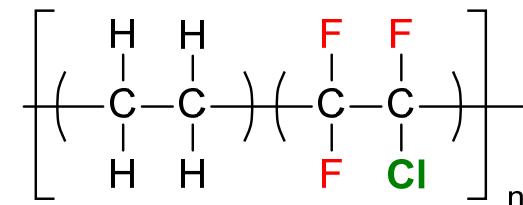
- similar performance
- lower gas crossover (factor $\times \sim 2$)

Further MEA (CCM)
development required

Can We Do Better Than That ?



ETFE (50 μm)



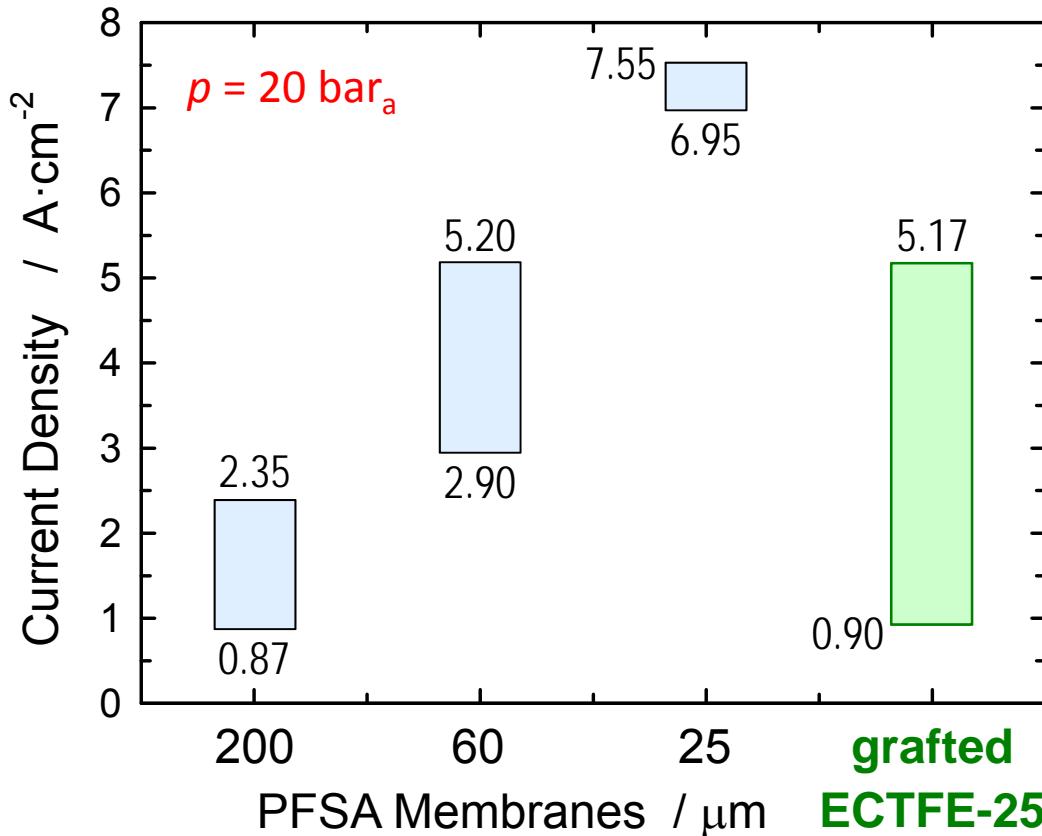
ECTFE (25 μm)

$$R_\Omega = 70 \text{ m}\Omega \cdot \text{cm}^2 \sim \text{Nafion 212}$$

$$i_x = 0.9 \text{ mA} \cdot \text{cm}^{-2} < \text{Nafion 117}$$

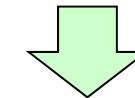
Thin membrane based on ECTFE-25 shows promising properties

Operational Range (Turndown Ratio)



i_{\min} = limit of 2% H_2 in O_2

- low Ohmic resistance
- low crossover



- wider range of operating current density
- suitable for **dynamic operation**

Cell tests to be done



Durability

Membrane Degradation Mechanisms

❖ Metal ion contamination (reversible)

- Water supply issue
- Corrosion of bipolar plates
- Core shell / alloy catalysts

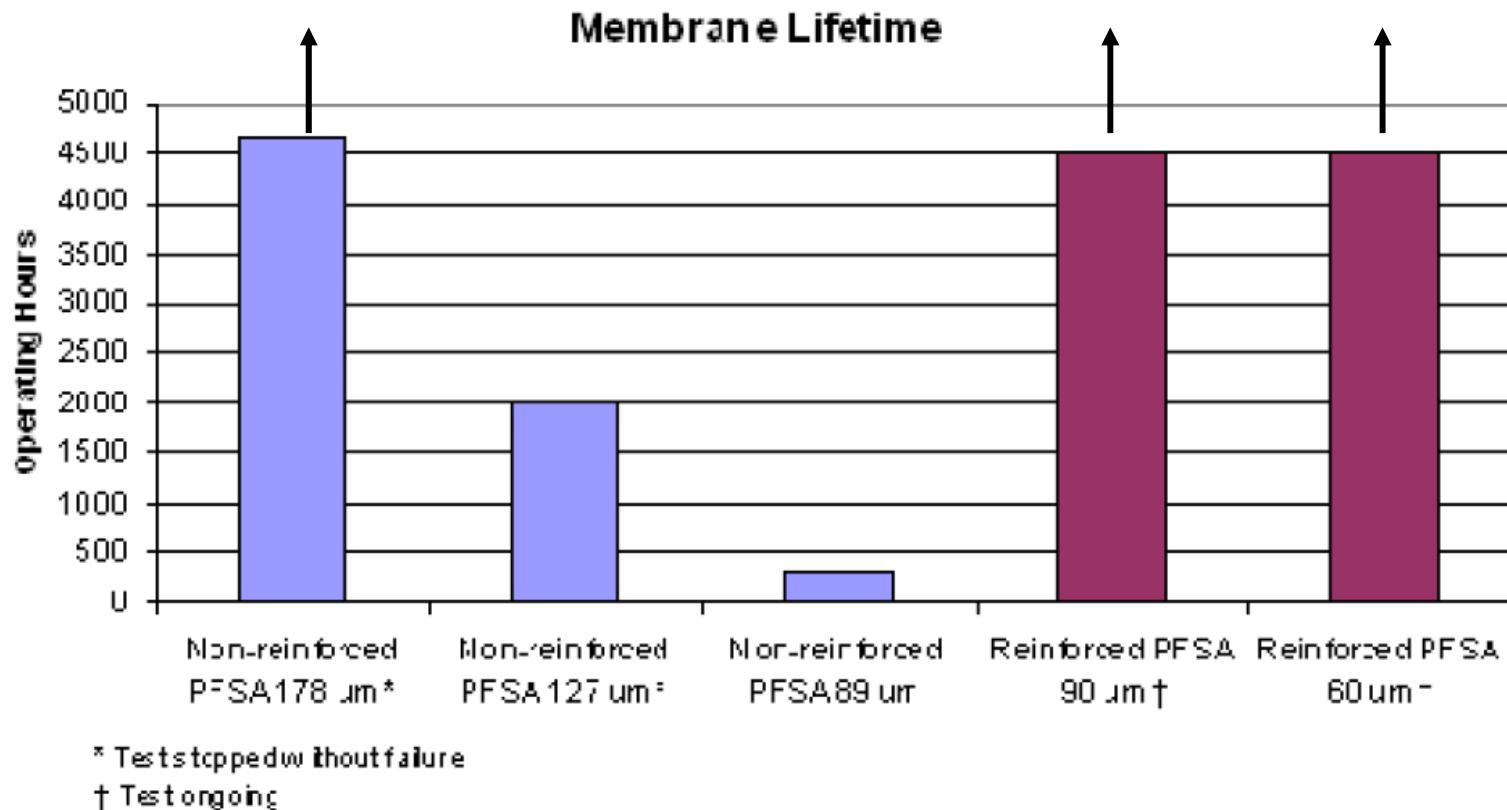
❖ Loss of mechanical integrity:

- Mechanical stress, creep
- Overall membrane thinning
- Local thinning

❖ Chemical degradation:

- H₂, O₂ crossover
- H₂O₂ and radical formation
- Fluoride release

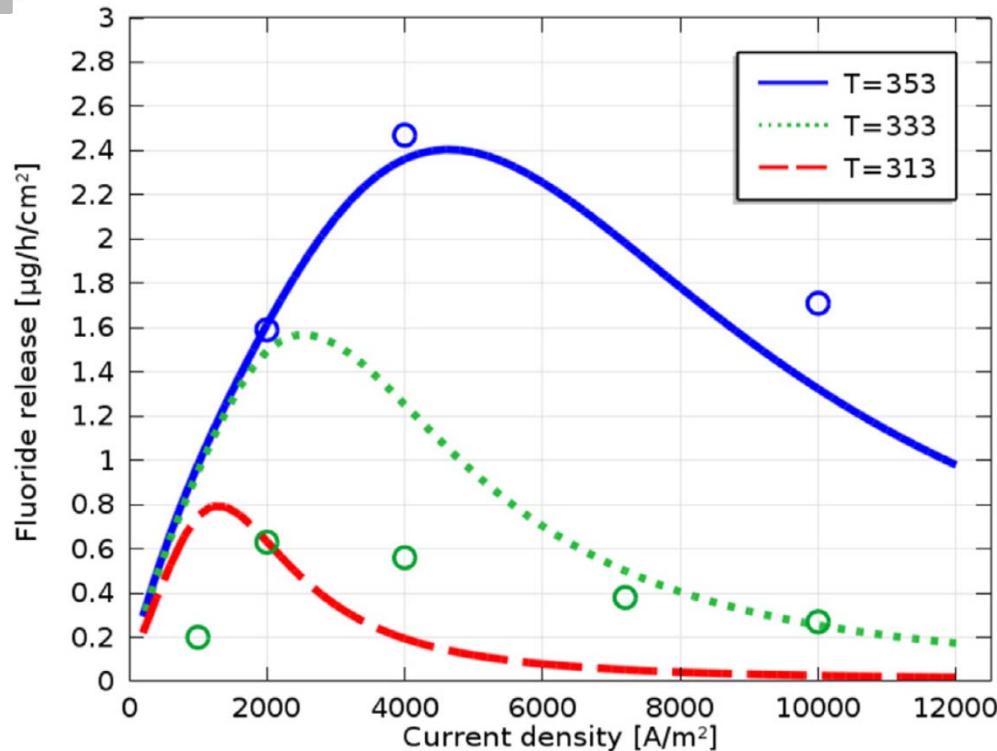
Membrane Degradation Mechanisms



Need accelerated stress tests

Contributions within NOVEL

Investigation of chemical degradation by measuring fluoride emission rate (FER) coupled to a degradation model



FER in the fuel cell*:

FC under load: $0.01 - 0.1 \mu\text{g}\cdot\text{cm}^{-2}\cdot\text{h}^{-1}$
FC under OCV: $1 - 10 \mu\text{g}\cdot\text{cm}^{-2}\cdot\text{h}^{-1}$

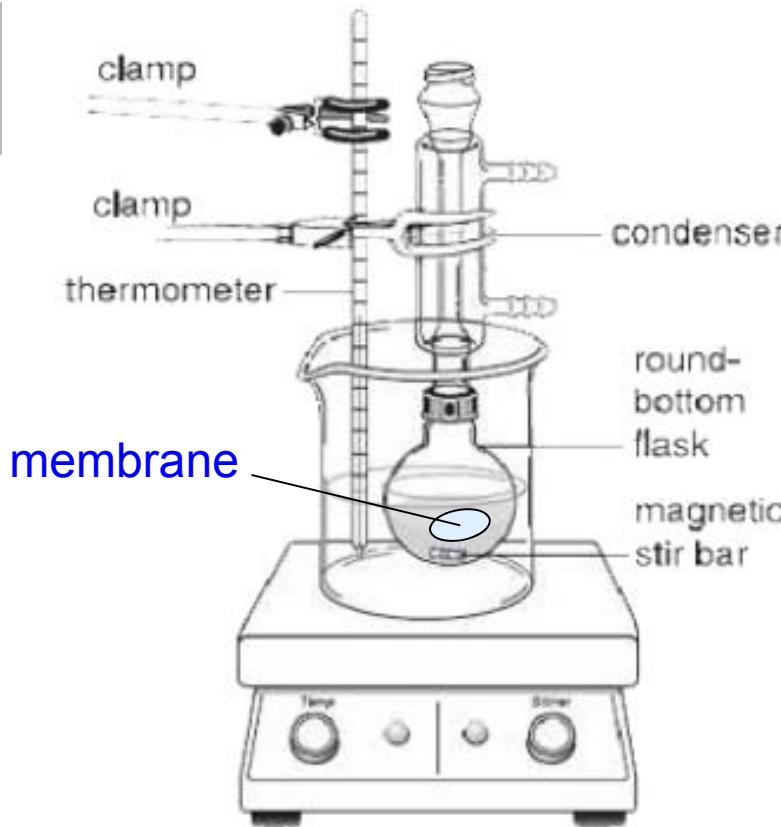
Shape of curve with maximum at intermediate current density well-reproduced by model

M. Chandesris et al., *Int. J. Hydrogen Energy* **40** (2015) 1353

* FER compilation in L. Gubler et al., *J. Electrochem. Soc.* **158** (2011) B755

Contributions within NOVEL

Thermal Stress Test (TST): exposure of membrane to 90°C for 5 days



post-test analysis of

membrane

- FTIR
- IEC
- SEM/EDX

solution

- UV-Vis
- Ion chromatography

| Membrane | IEC loss (%) |
|----------------------------|----------------|
| grafted, initial design | 44.2 ± 0.8 |
| down-selected grafted | 4.2 ± 0.5 |
| Nafion 117 | < 1 |

A. Albert et al., in preparation

Conclusions

- ❖ Operation over large current density range desired
- ❖ Resistance - crossover tradeoff for a given ionomer type
- ❖ Strategies for improved membranes in NOVEL
 - Modified PFSA membranes (reinforced, with recombination catalyst)
 - Other ionomer classes with superior combination of resistance and gas barrier properties
- ❖ Durability aspects tackled within NOVEL
 - Radical induced degradation: model and experiment
 - Thermal stress test at 90°C in water

Thank You

