

Contribution to the analysis of the corrosion process of commercial steels and newly developed laboratory alloys under simulated incineration conditions

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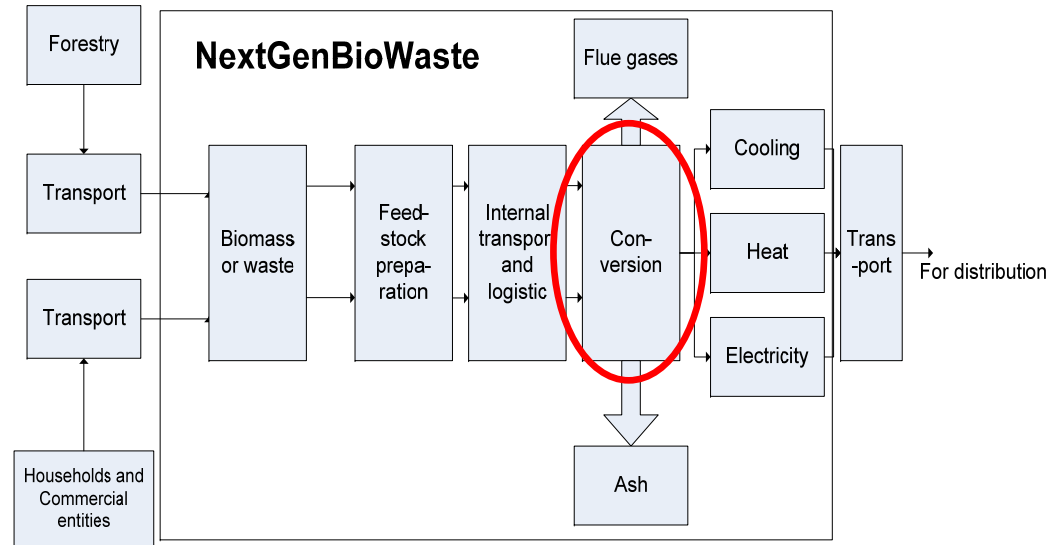
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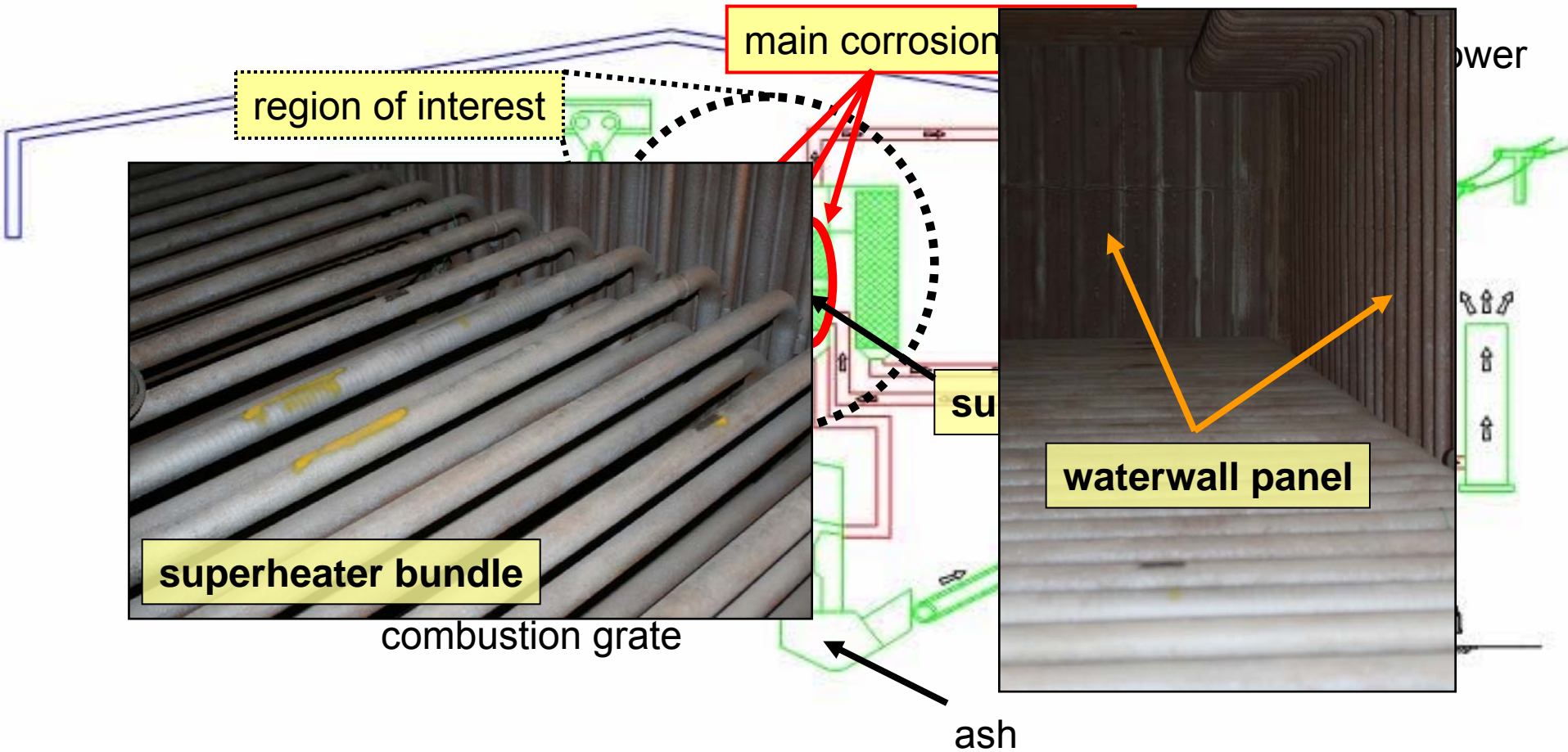
NGBW covers the supply chain:

- SP 1: Fuel preparation
- **SP 2: Conversion**
- SP 3: Residue handling
- SP 4: Wholesale of energy



NGBW objectives SP 2: [excerpt]

- in general: innovative technologies to improve the corrosion resistance with the result of improved energy recovery, reliability and performance of waste and biomass combustion plants
- enhanced process conditions in order to achieve a higher efficiency
 - reduction of corrosion and fouling problems
 - ⇒ improving boiler materials in order to withstand HTC
 - ⇒ advanced boiler materials and new protecting coatings
- reducing maintenance costs by use of more corrosion resistant, but cost-effective materials and coatings
 - target: double lifetime of heat exchange components at existing steam temperatures

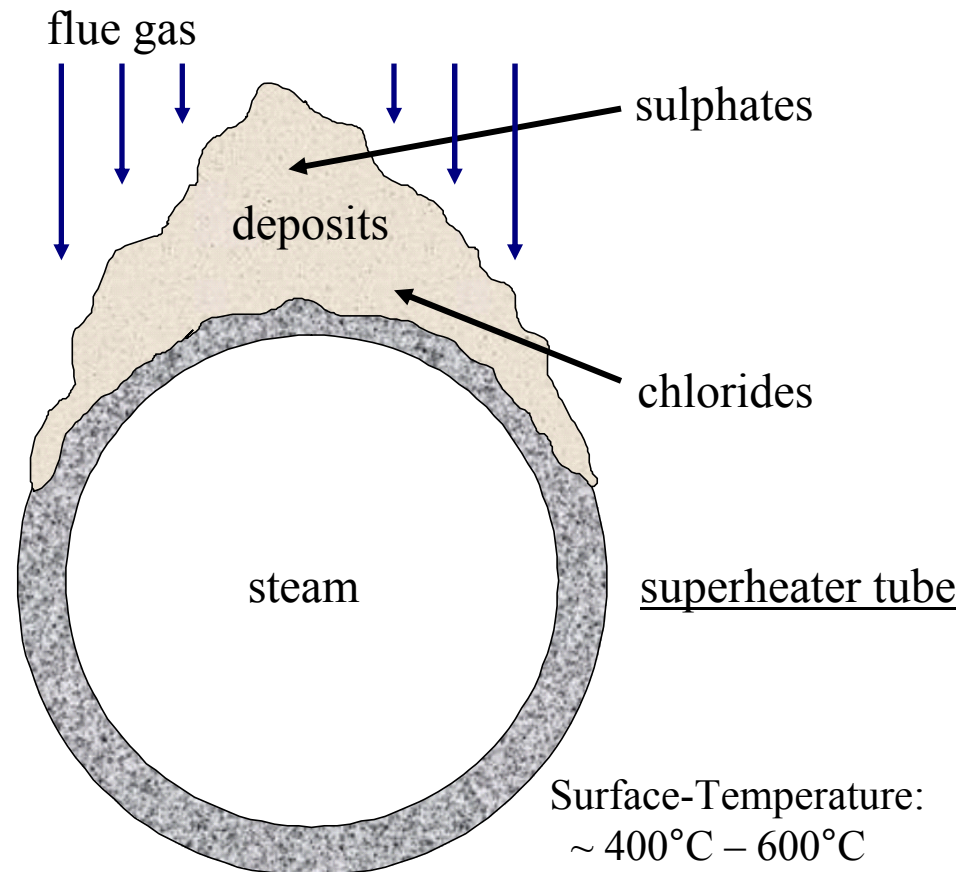


Deposit constituents on WtE superheater in wt.-% [excerpt]

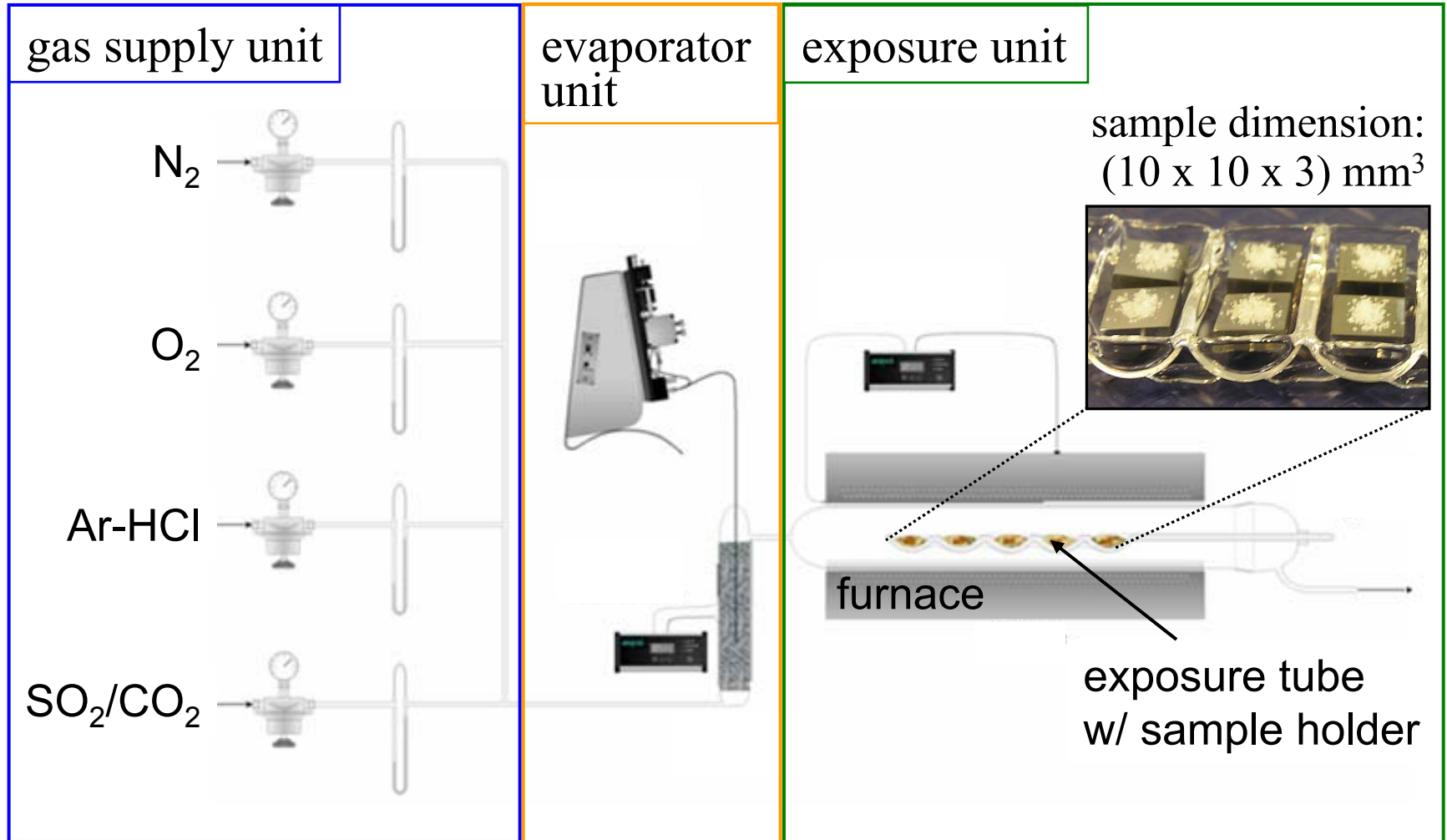
	Na ⁺	K ⁺	Ca ²⁺	Pb ²⁺	Zn ²⁺	SO ₄ ²⁻	Cl ⁻
No 1	4.1	7.6	12.5	7.4	2.3	28.0	0.5
No 2	2.4	3.8	13.0	1.6	9.7	16.6	1.2

Flue gas concentration [excerpt]

Species	Concentration [vppm]	
HCl	560.0	2240.0
SO ₂	35.0	700.0
SO ₃	1.4	19.6
NO ₂	71.5	214.5
CO	64.0	640.0
Pb	1.1	6.5
Zn	3.5	51.7



- Lab-scale testing of materials and validation of testing methods using plant exposures



- Gases (based on PREWIN conditions)

	HCl	SO ₂	CO ₂	H ₂ O	O ₂	N ₂
Waste	2,000 vppm	200 vppm	-	15 vol.-%	8 vol.-%	Bal.
Biomass	200 vppm	-	13 vol.-%	22 vol.-%	5 vol.-%	Bal.

- Synthetic deposits

	Na ₂ SO ₄	K ₂ SO ₄	CaSO ₄	ZnSO ₄	KCl	ZnCl ₂
Waste/biomass superheater	33 wt.-%	33 wt.-%	33 wt.-%			
Waste/biomass superheater		50 wt.-%			50 wt.-%	
Waste superheater	25 wt.-%	25 wt.-%	25 wt.-%	25 wt.-%		
Waste water wall					50 mol.-%	50 mol.-%

	Material	Cr	Ni	Mo	Mn	Other
Low Cr-steels	15Mo3	–	–	0.30	0.52	C 0.16; Si 0.26
	13CrMo4 4	0.96	0.07	0.48	0.46	C 0.12; Si 0.21
	10CrMo9 10 (T22)	2.10	–	0.92	0.43	C 0.12; Si 0.22
	7CrWMoVNb9 6 (T23)	2.3	–	0.15	0.27	C 0.06; Si 0.15; V 0.2; W 1.58 ; Nb 0.06; B 0.005; N 0.02; Al 0.02
High Cr-steels	X20CrMoV12 1	10.45	0.70	0.88	0.60	C 0.18; Si 0.22; V 0.26
	X10CrWMoVNb9 2 (T92)	9.15	0.26	0.50	0.46	W 1.70 ; Si 0.22; Nb 0.6; N 0.05; V 0.2; B 0.003; C 0.11
High Cr-/Ni-steels	Esshete 1250	14.90	9.65	0.94	6.25	C 0.084; Si 0.58; Nb 0.86; V 0.22; B 0.004
	TP 347 H	17.60	10.70	–	1.84	Si 0.29; C 0.05; Nb 0.6
	Sanicro 28	27.00	31.00	3.50	≤ 2.00	C 0.02; Si 0.07; Cu 1.0
Ni-base alloy	Inconel 625	22.00	Bal.	9.00	–	Fe 3.0; Nb 3.5; C 0.025

- Modified 9%Cr-Steels (P91/T92)

Material [wt.-%]	Cr	Al	Si	Ni
Fe-9Cr-5Al	9.0	5.0	-	-
Fe-9Cr-2.5Al-2.5Si	9.0	2.5	2.5	-
Fe-9Cr-5Ni-2.5Al-2.5Si	9.0	2.5	2.5	5.0

- Iron Aluminides

Material [at.-%]	Al [wt.-%]	Fe
Fe-15Al	7.9	bulk
Fe-26Al	14.5	bulk
Fe-40Al	24.4	bulk

α -Fe, Al: disordered A2

Fe₃Al: ordered D0₃ (600°C B2)

FeAl: ordered B2



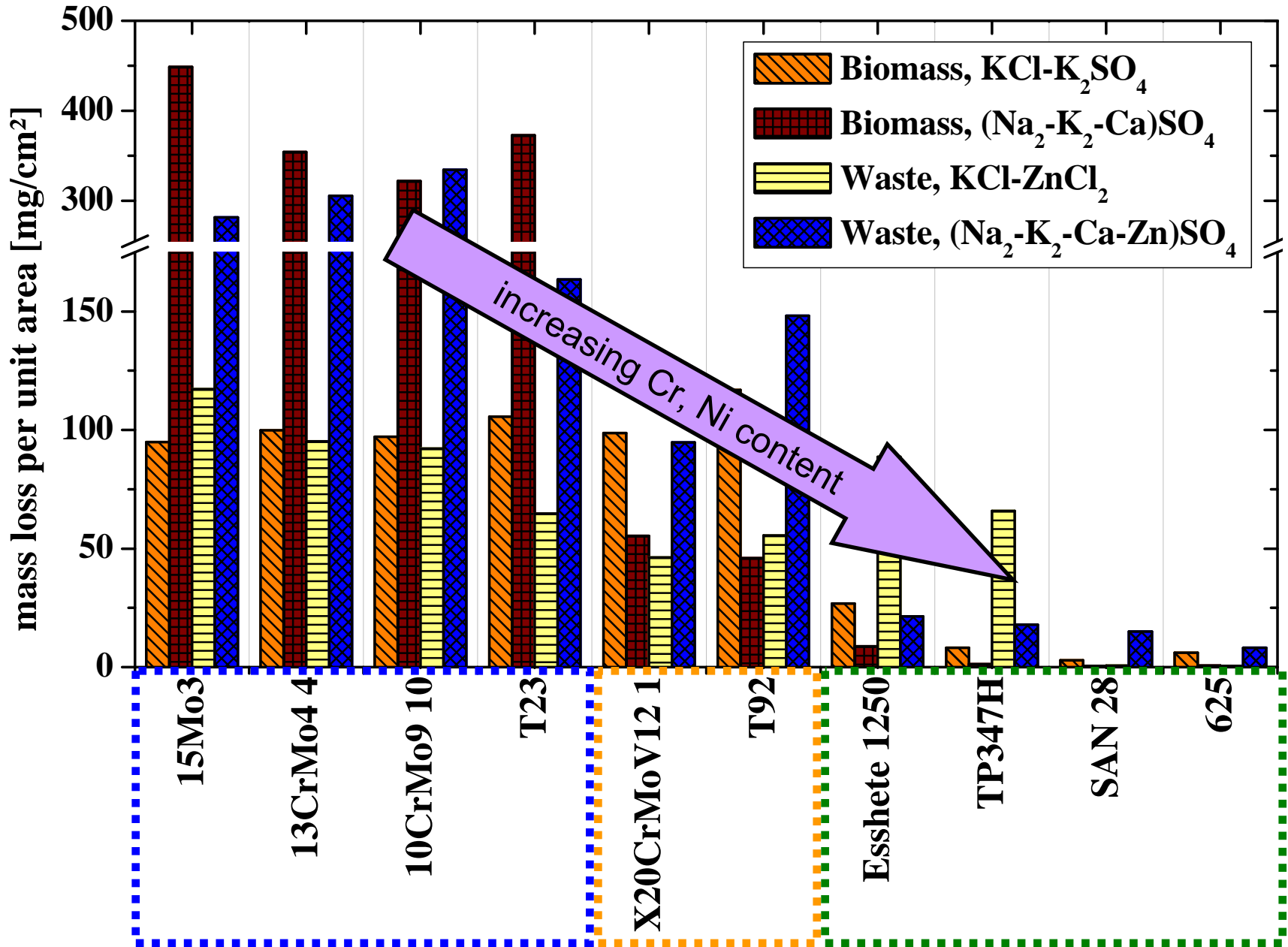
- 9-12%Cr ferritic-martensitic steels:
 - High strength and creep resistant steels suitable for use at temperatures up to 650°C
- Coatings/alloy composition modification in Cr, Si, Al will improve corrosion resistance
- Cr will enable and promote the outwards diffusion of Al
- Cr-reservoir reduces Al/Si-amount needed to maintain external alumina or silica scale
- Alumina scales are not as severely affected by steam as chromia, silica
- > 5wt.% Cr, Si → too high for industrial applications considering detrimental effects on metallurgical and mechanical properties



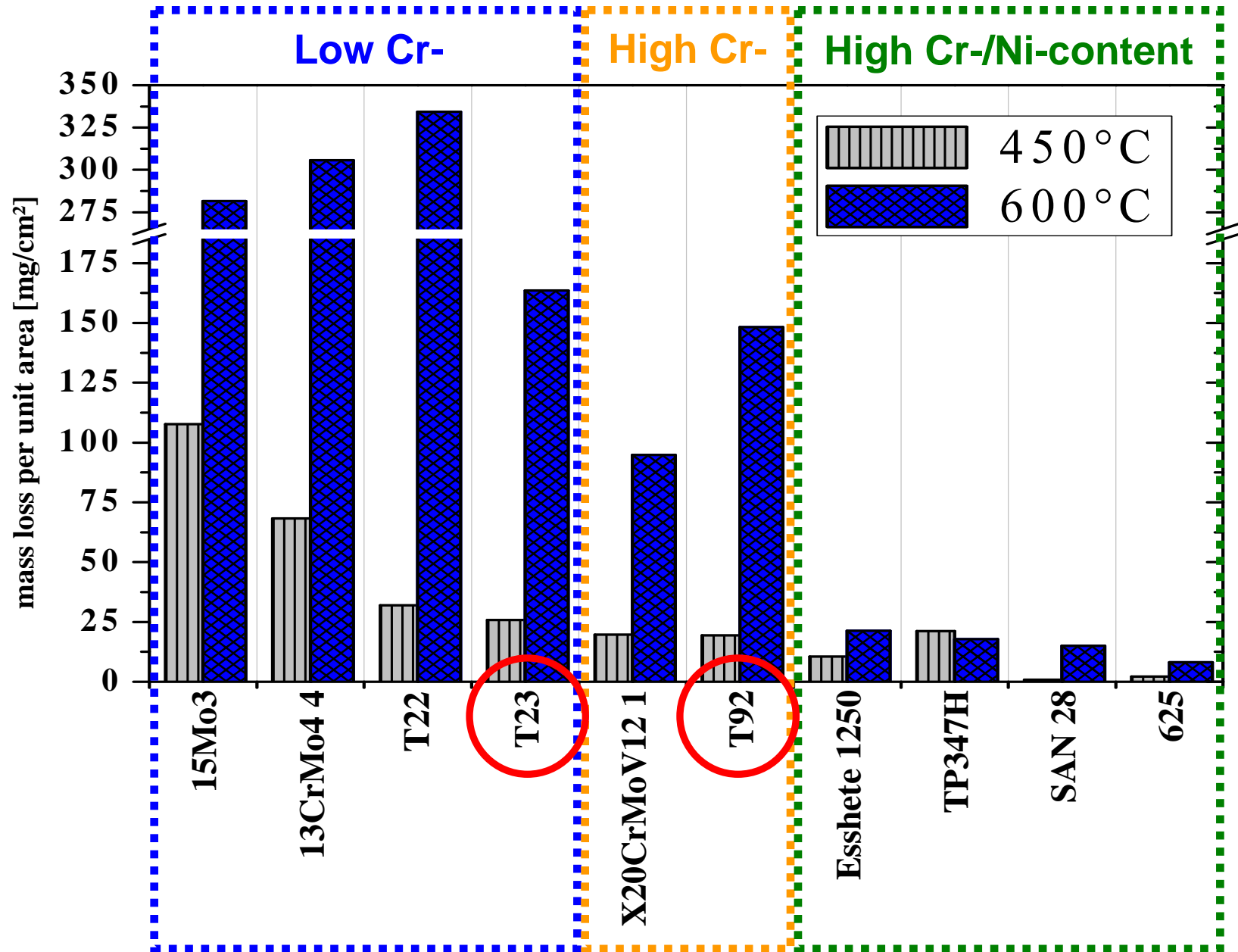
- ☺ Superior corrosion resistance in oxidising/sulphidising atmosphere
- ☺ Much improved corrosion resistance under molten salt compared to Fe-Cr alloys
- ☺ Light-weight structural materials
- ☺ Recent efforts led to Fe-Al alloys have the potential to be used for structural applications at least between 650-800°C
- ☺ Development and improvement of Fe₃Al and FeAl concerning high strength, high ductility and high creep resistance between 500-1,000°C
- ☺ Fe-Al-X alloys show better creep rates than P92

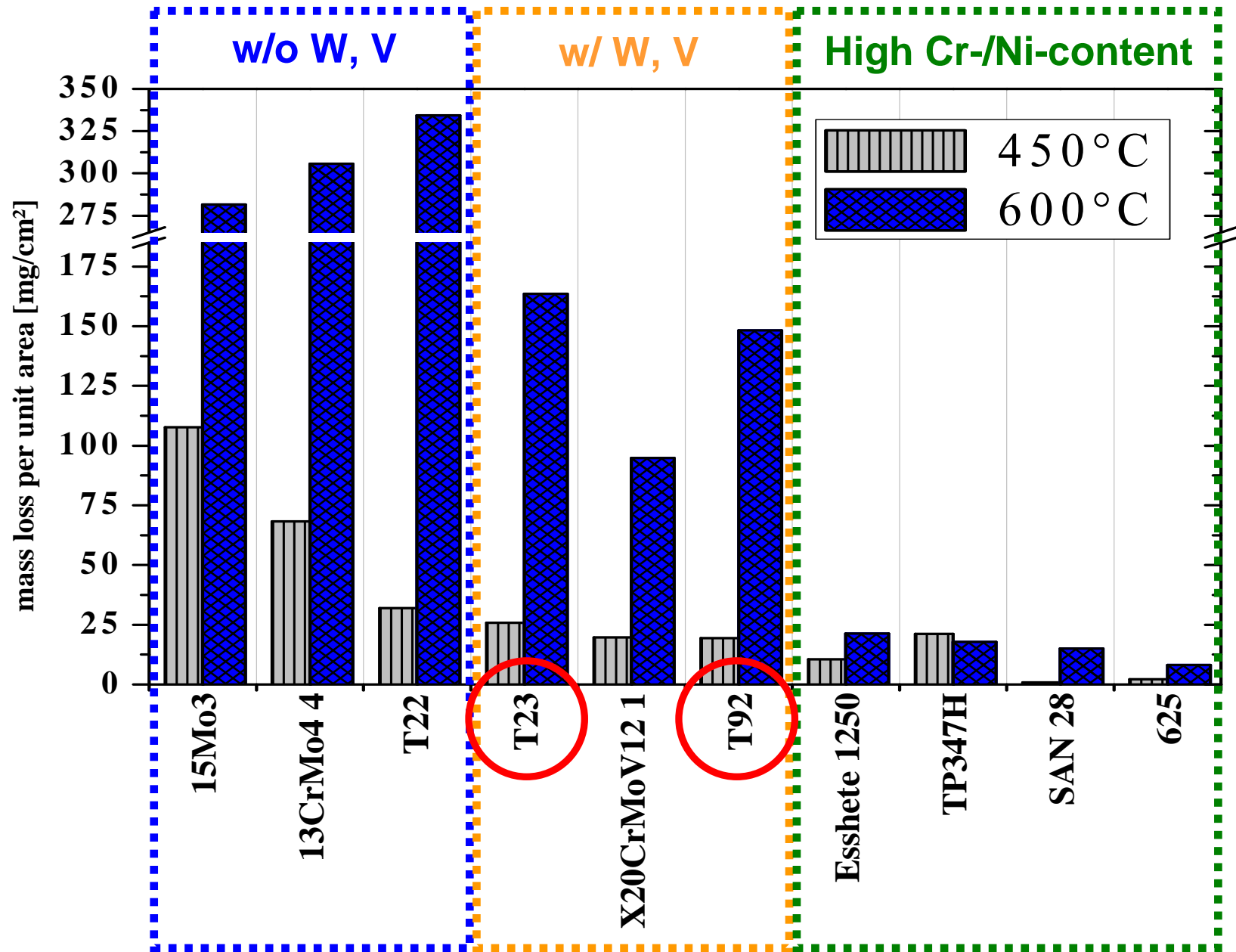
Corrosion Test: Commercial Steels

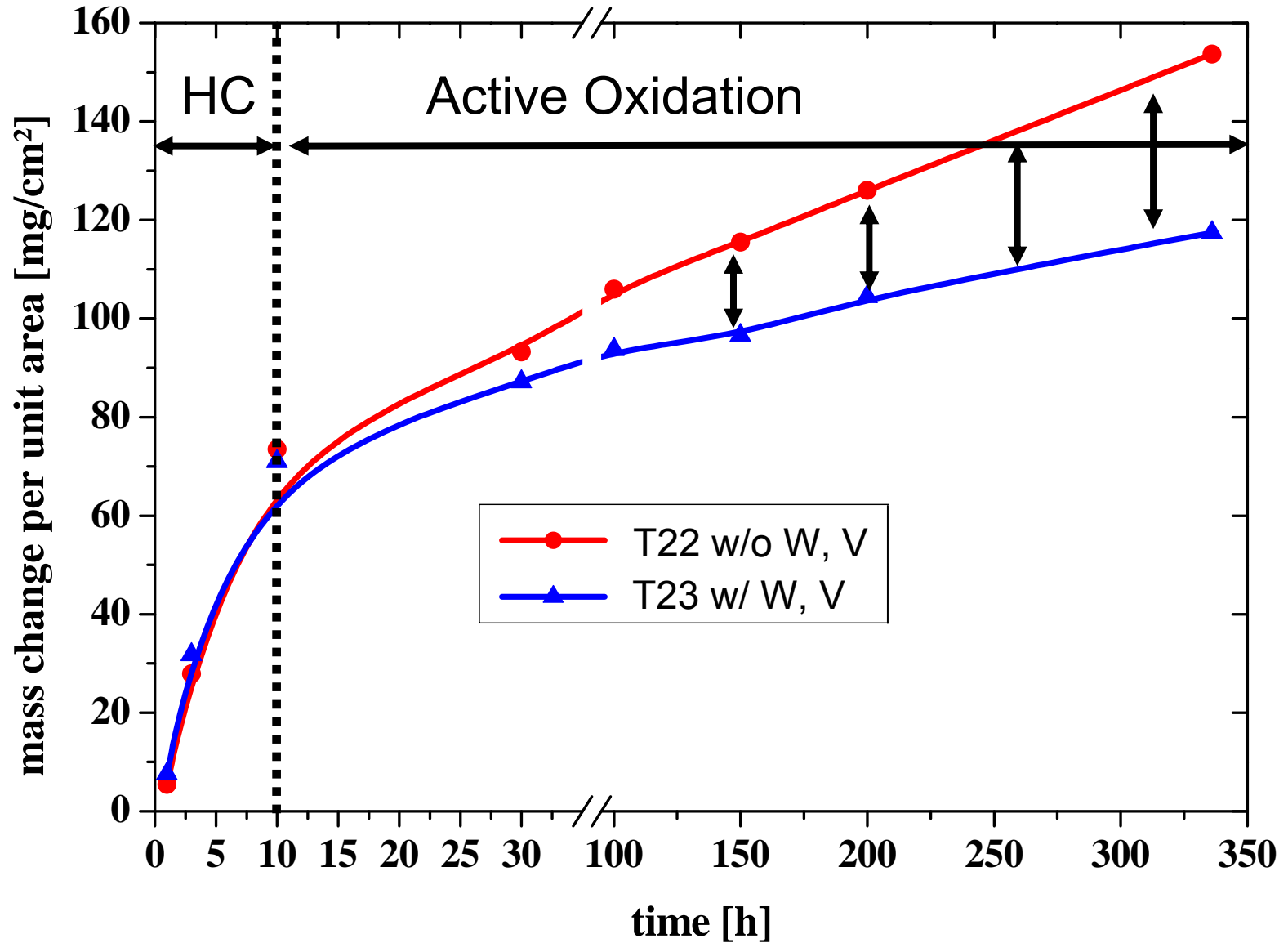
Corrosion Tests at 600°C for 336 h



Waste, $(\text{Na}_2\text{-K}_2\text{-Ca-Zn})\text{SO}_4$, 600°C, 336 h

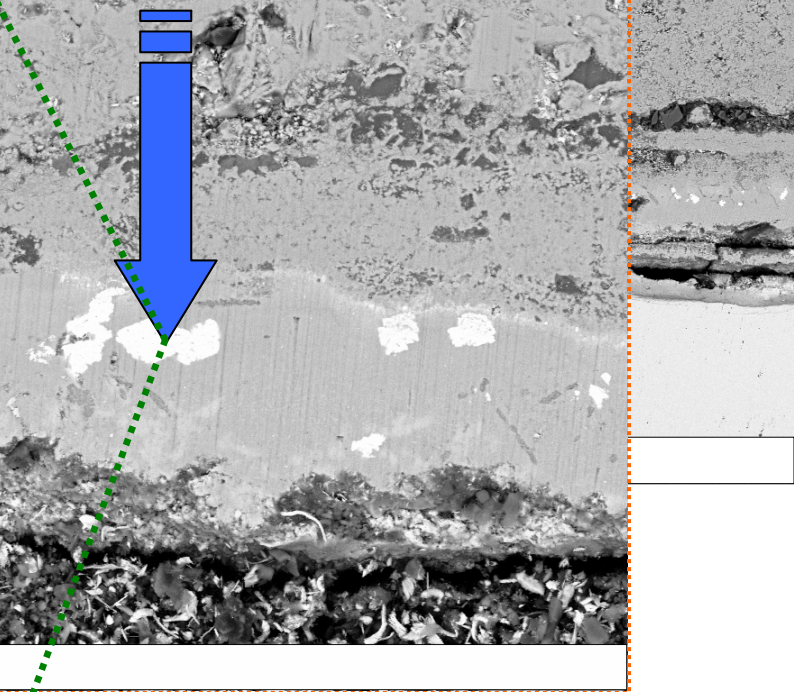
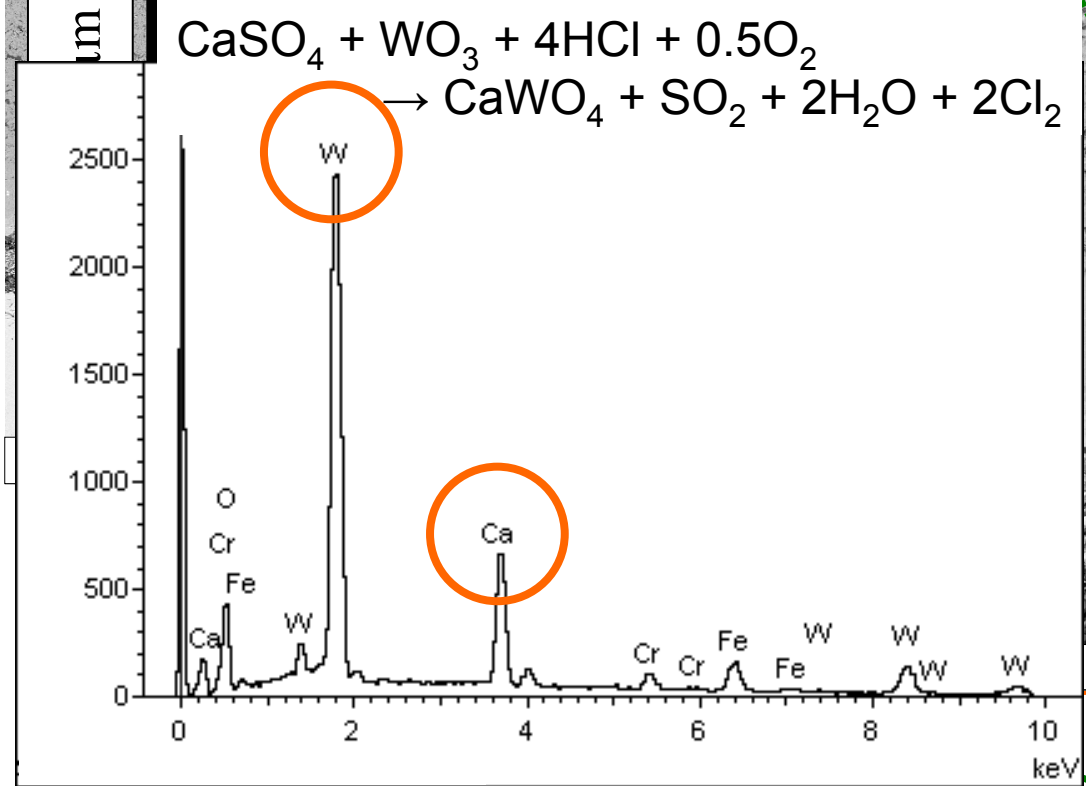
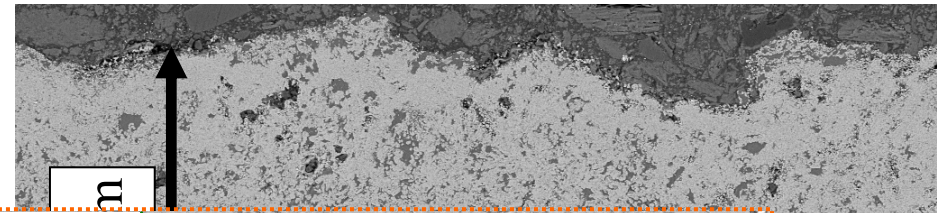
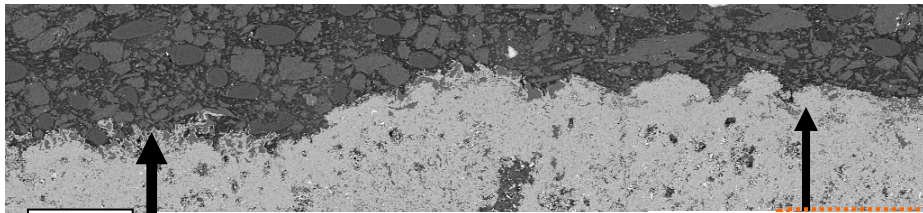


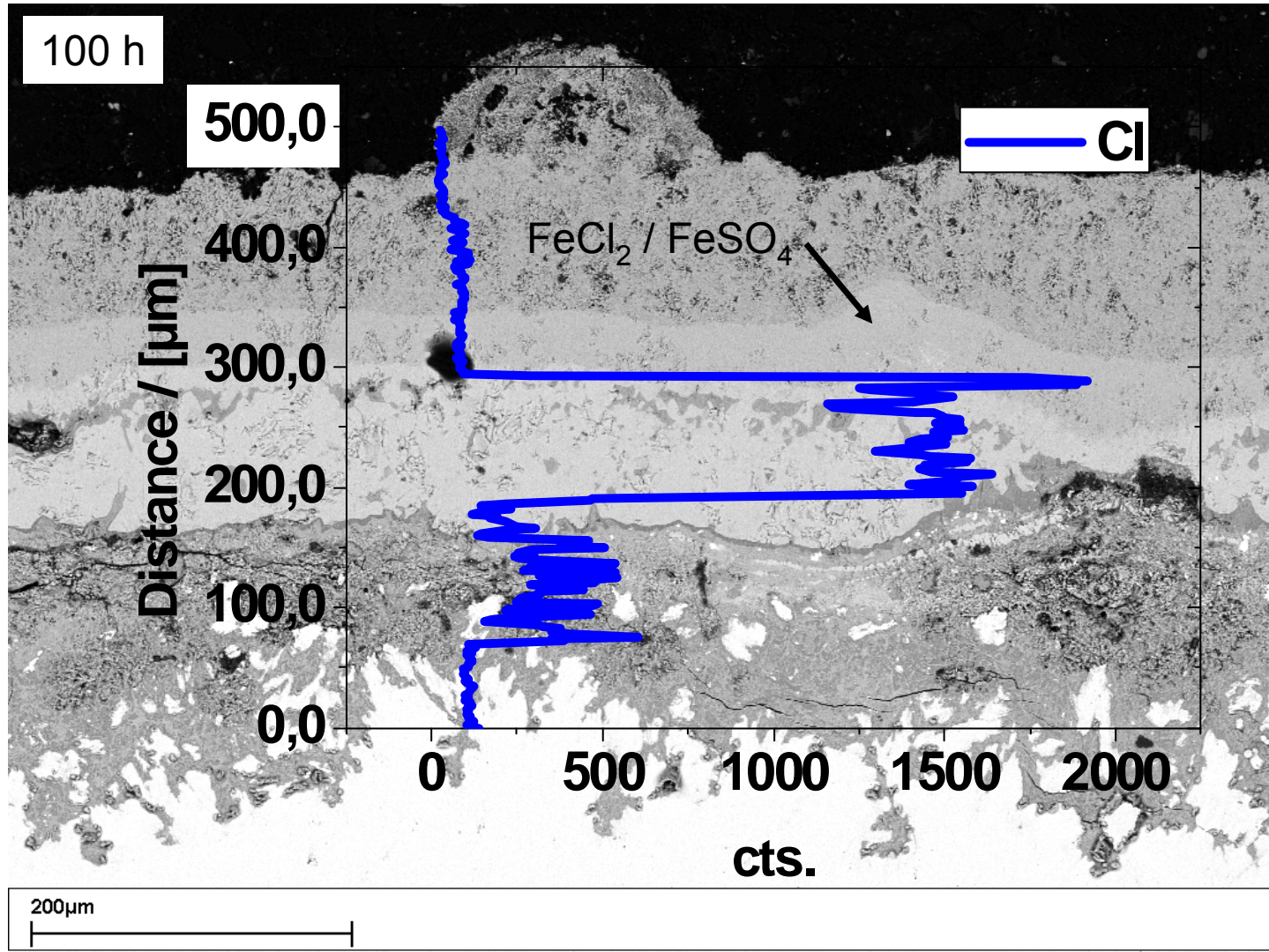


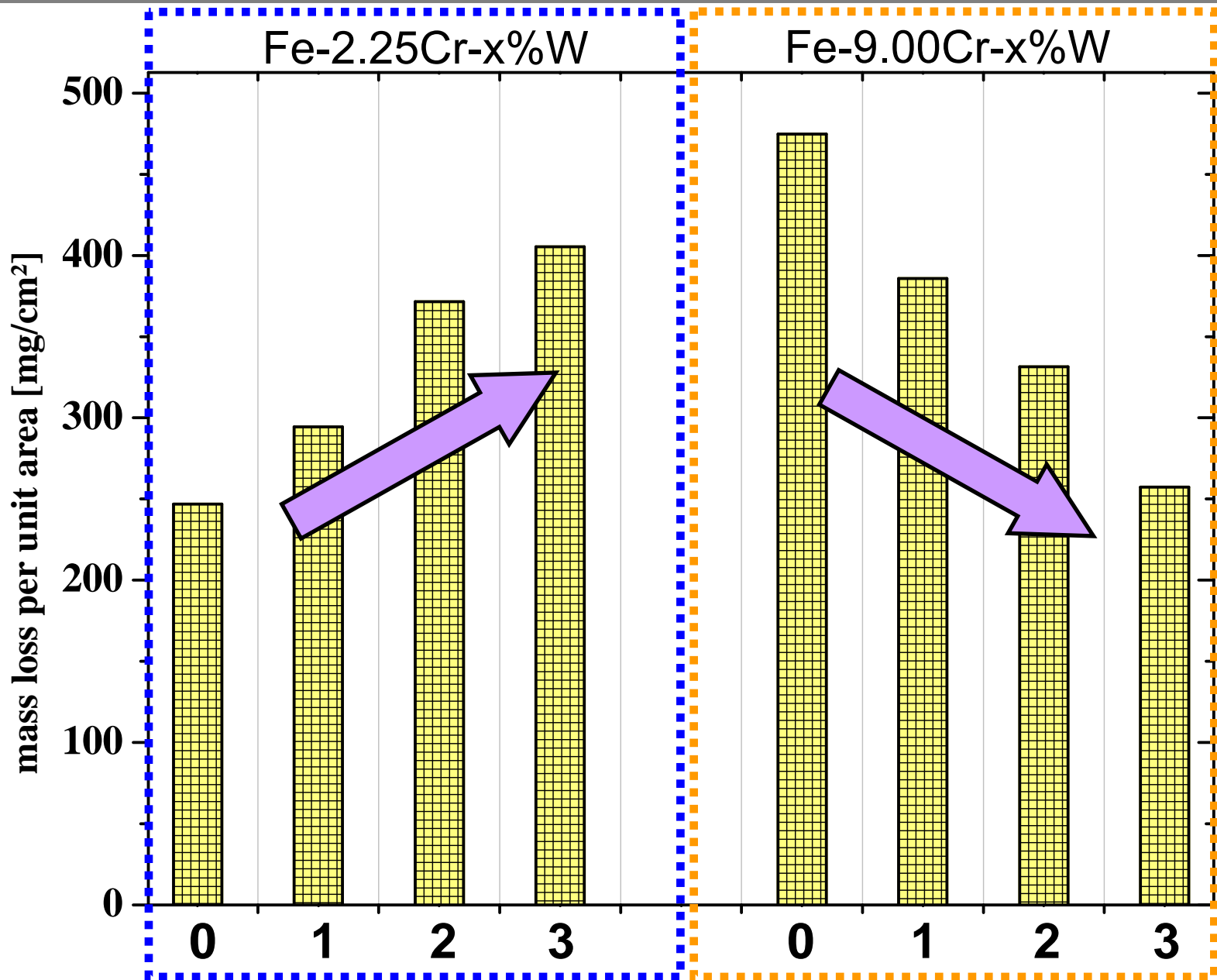


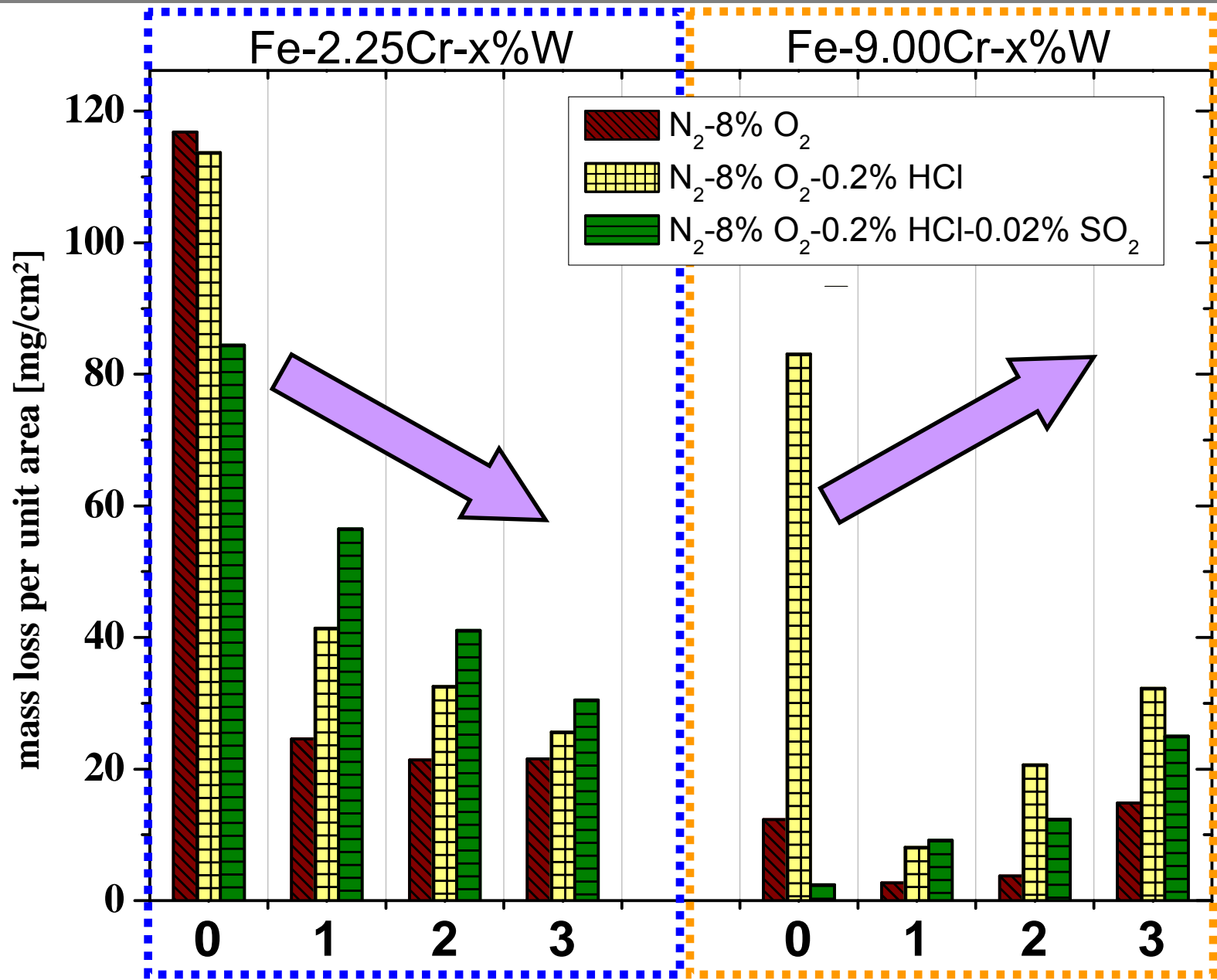
Low alloyed steel: **T23**

High alloyed steel: **T92**

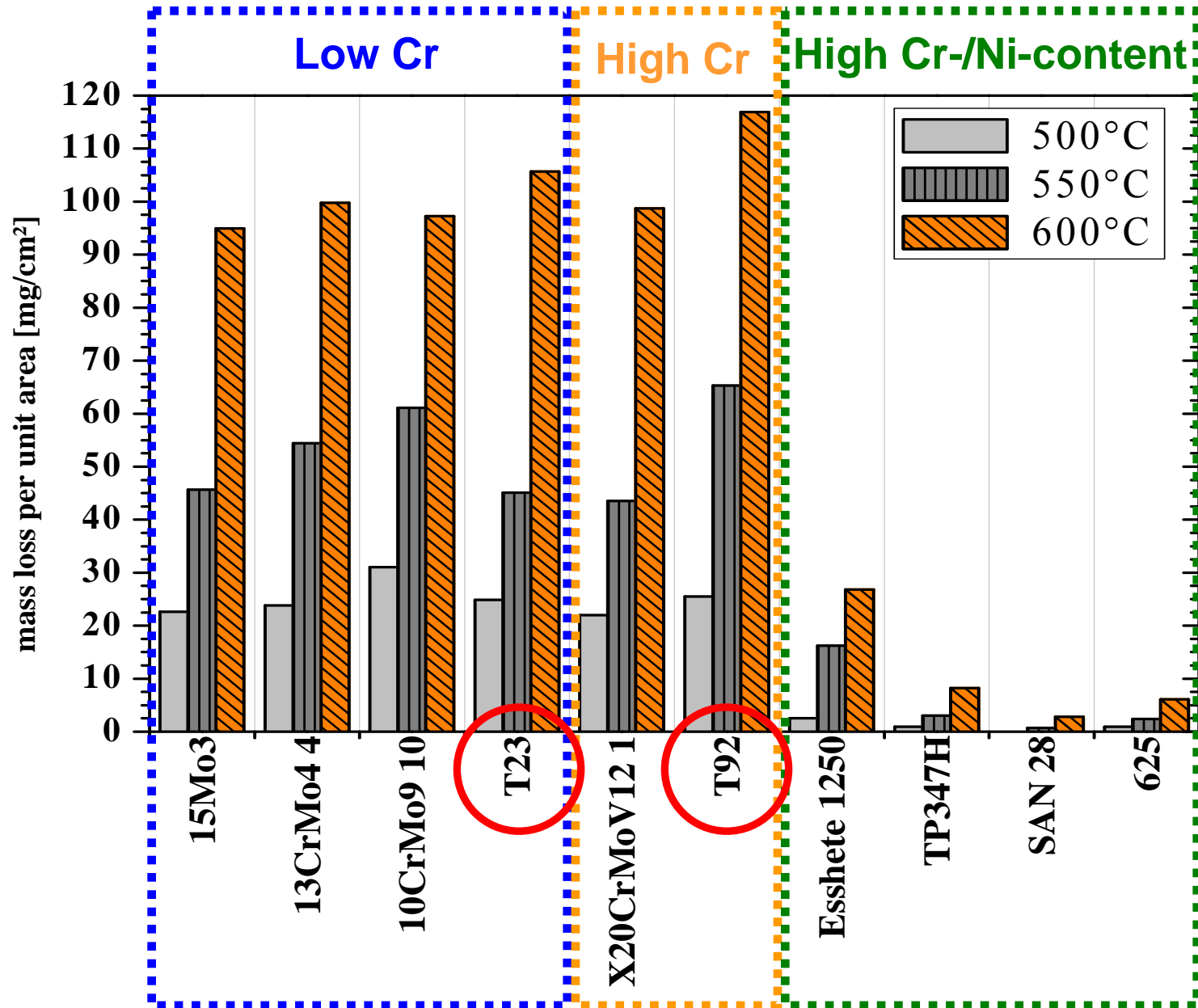


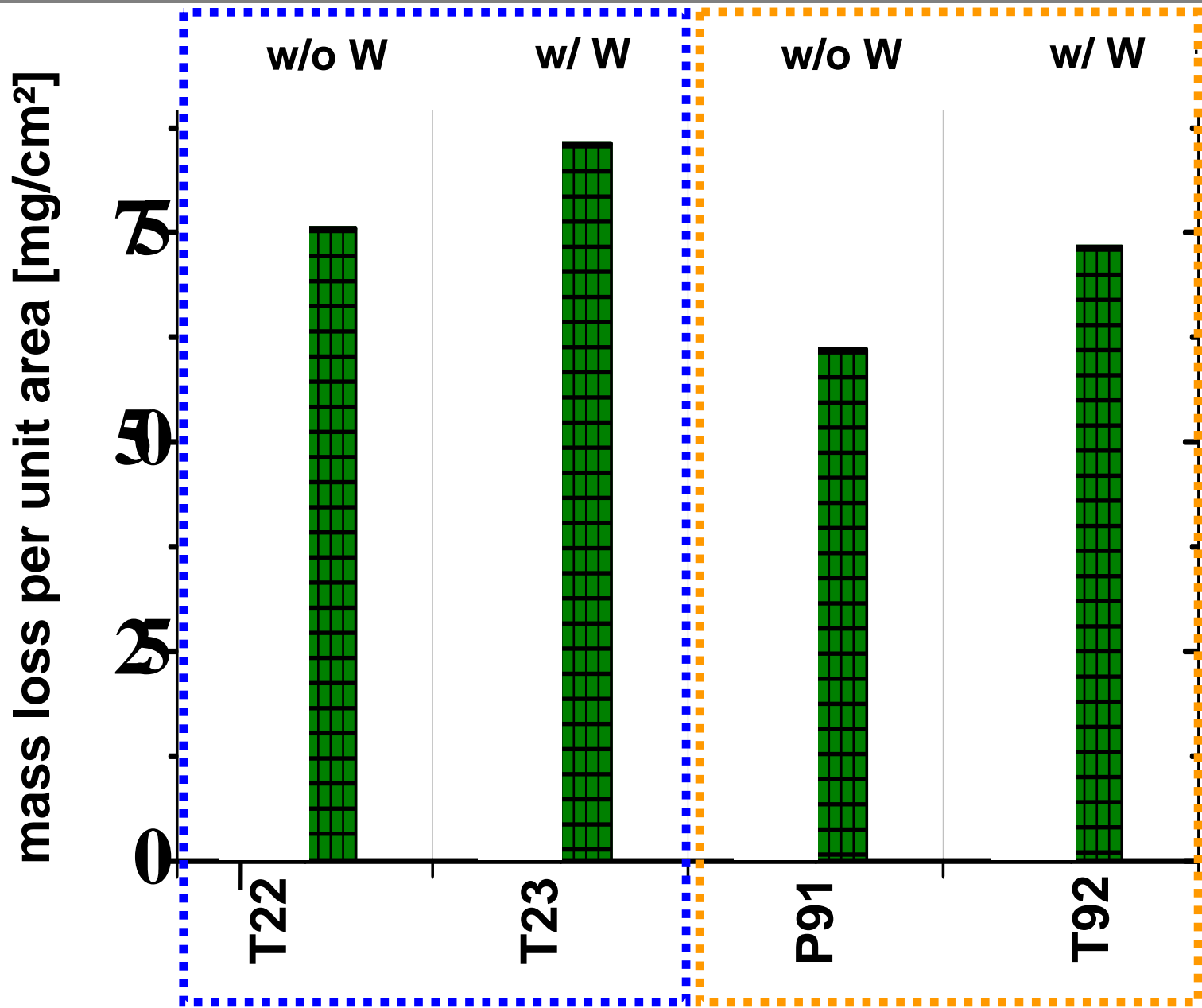






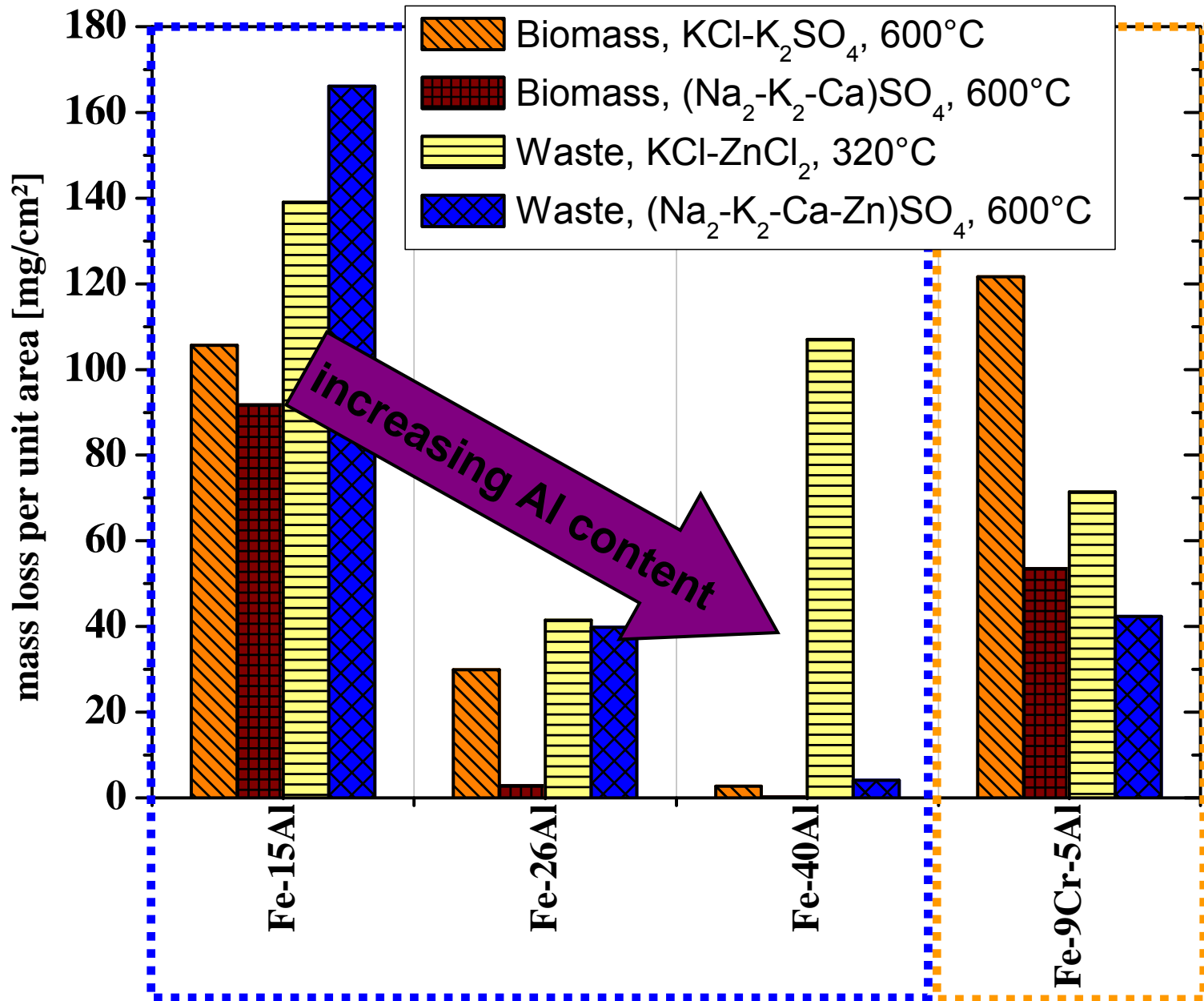
Biomass, KCl-K₂SO₄, 600°C, 336 h



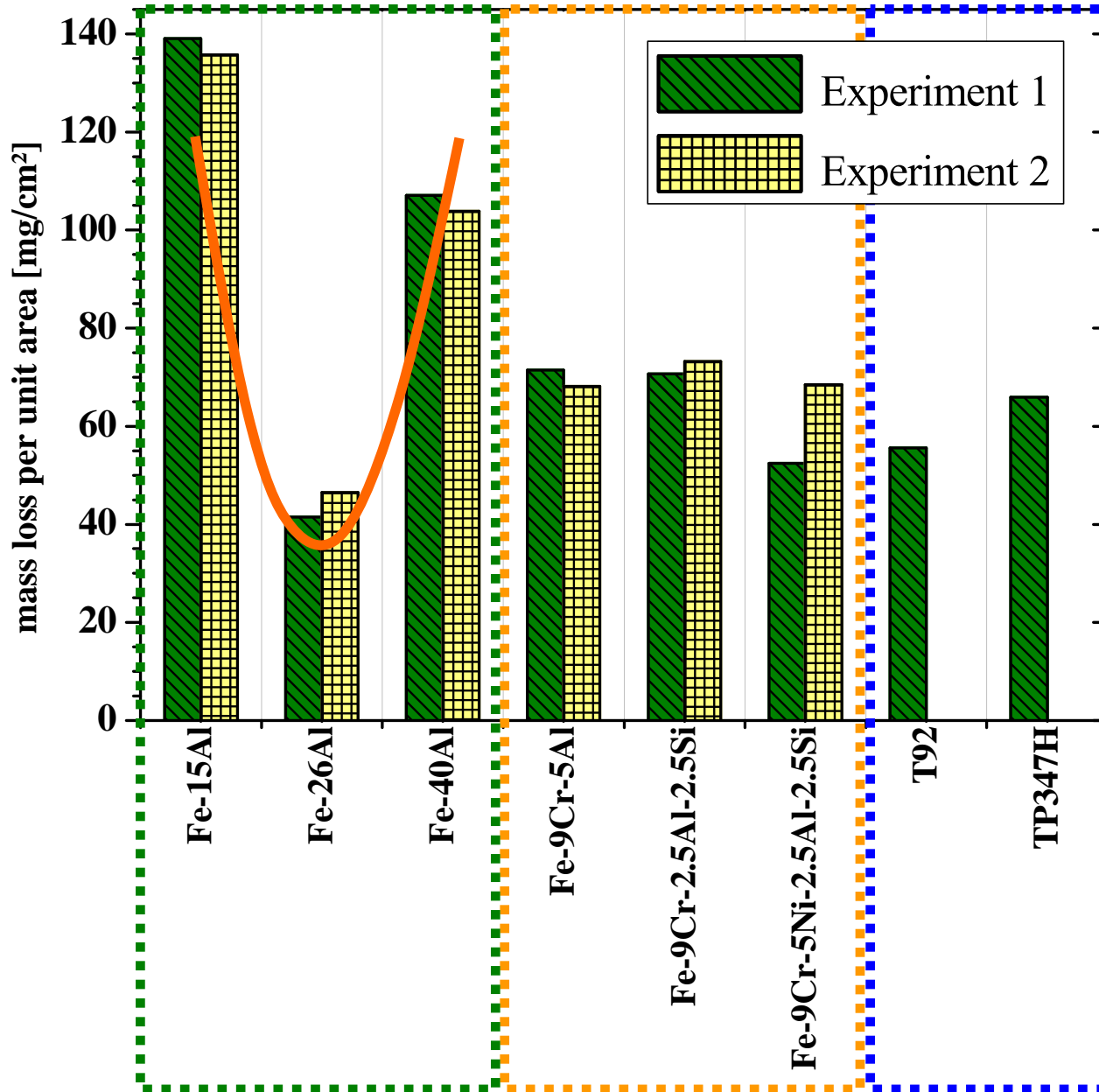


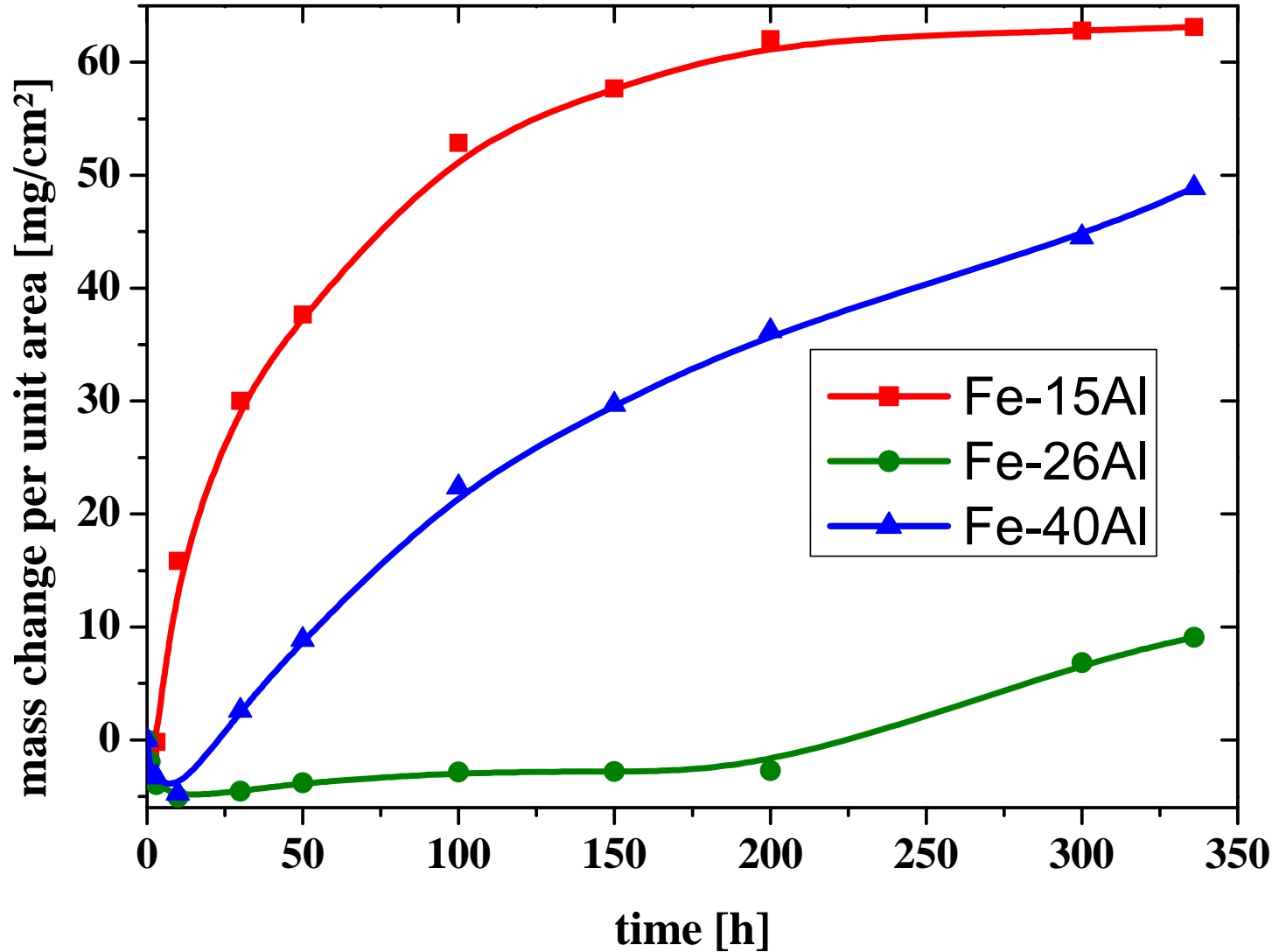
Corrosion Test: Modified 9%Cr-Steels / FeAl

Summary: Corrosion Tests Fe-Al for 336 h

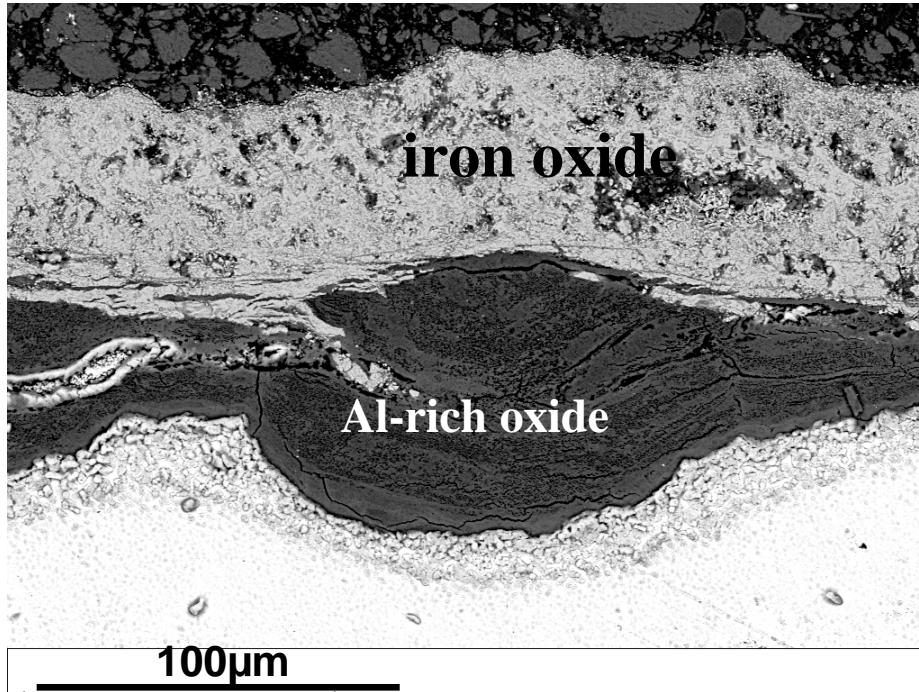


Waste, KCl-ZnCl₂, 320°C, 336 h

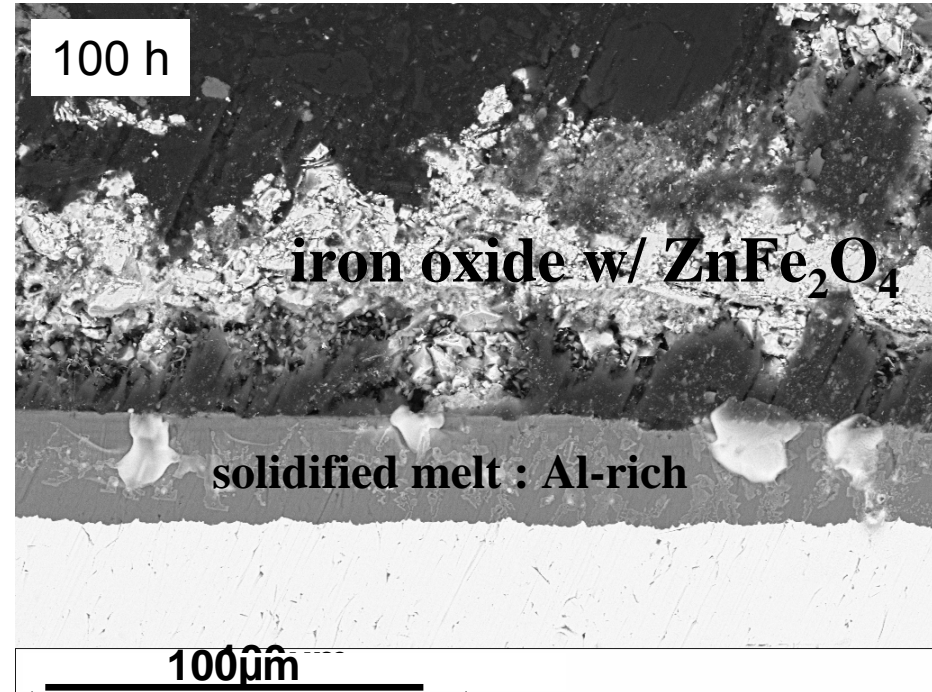


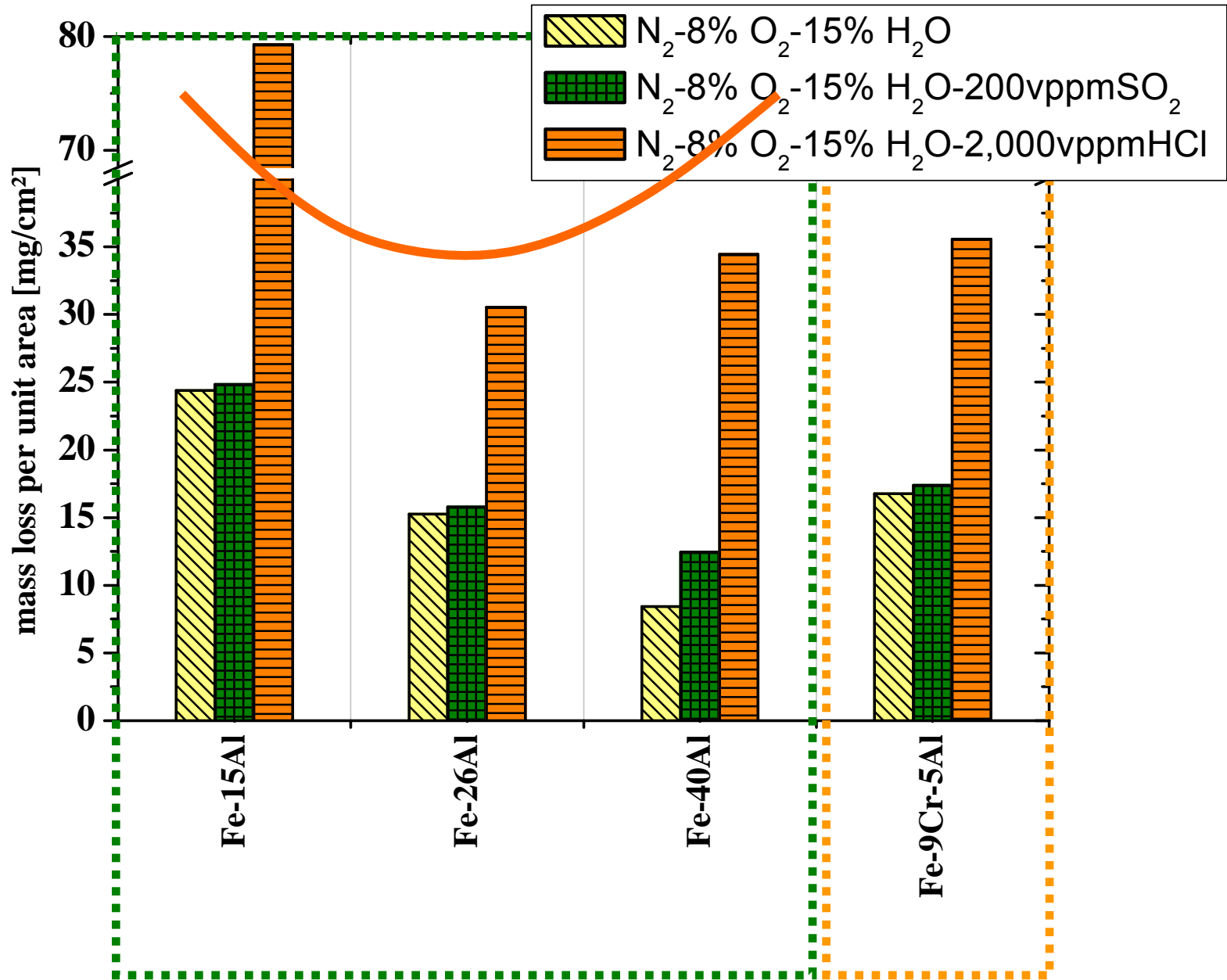


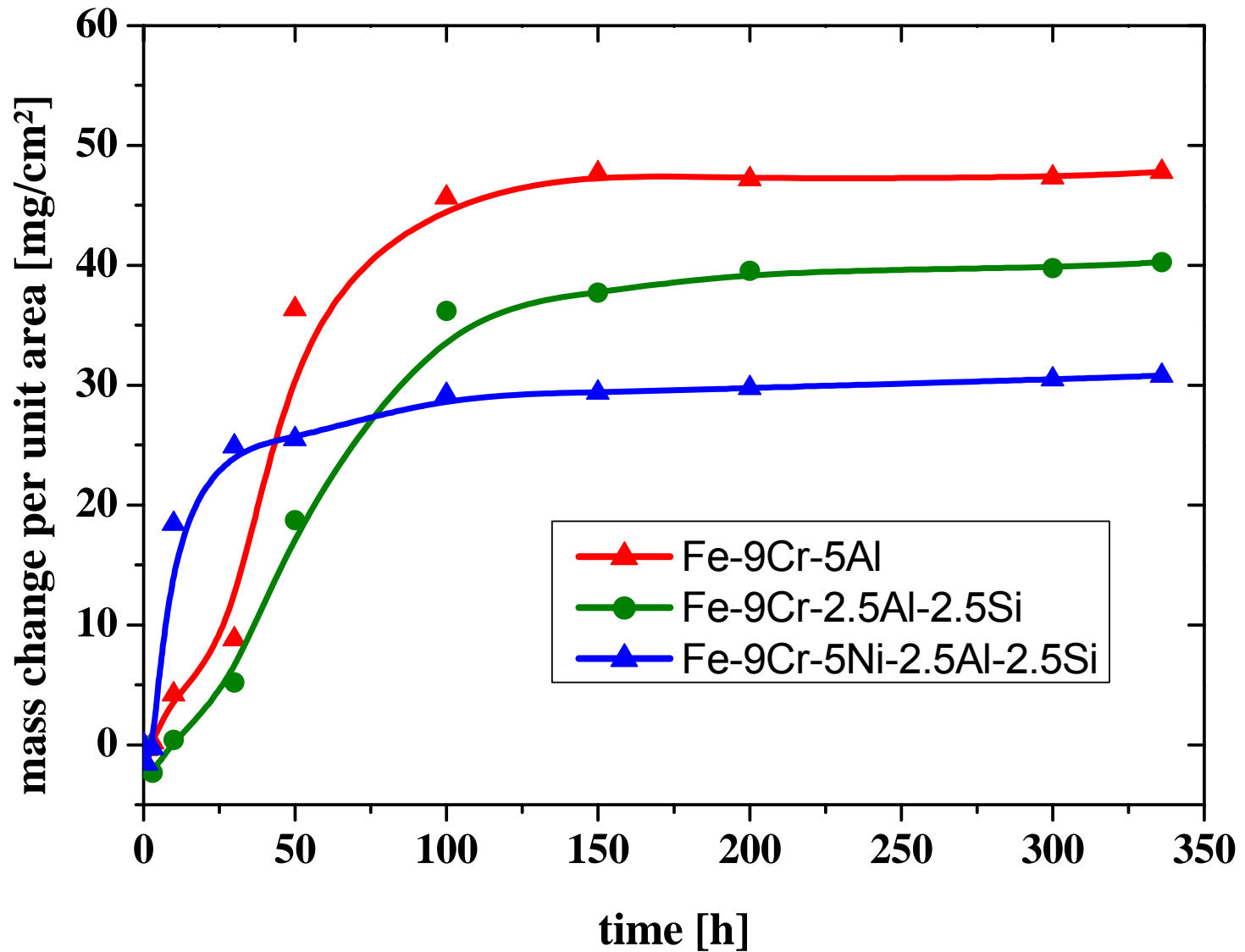
Fe-26Al

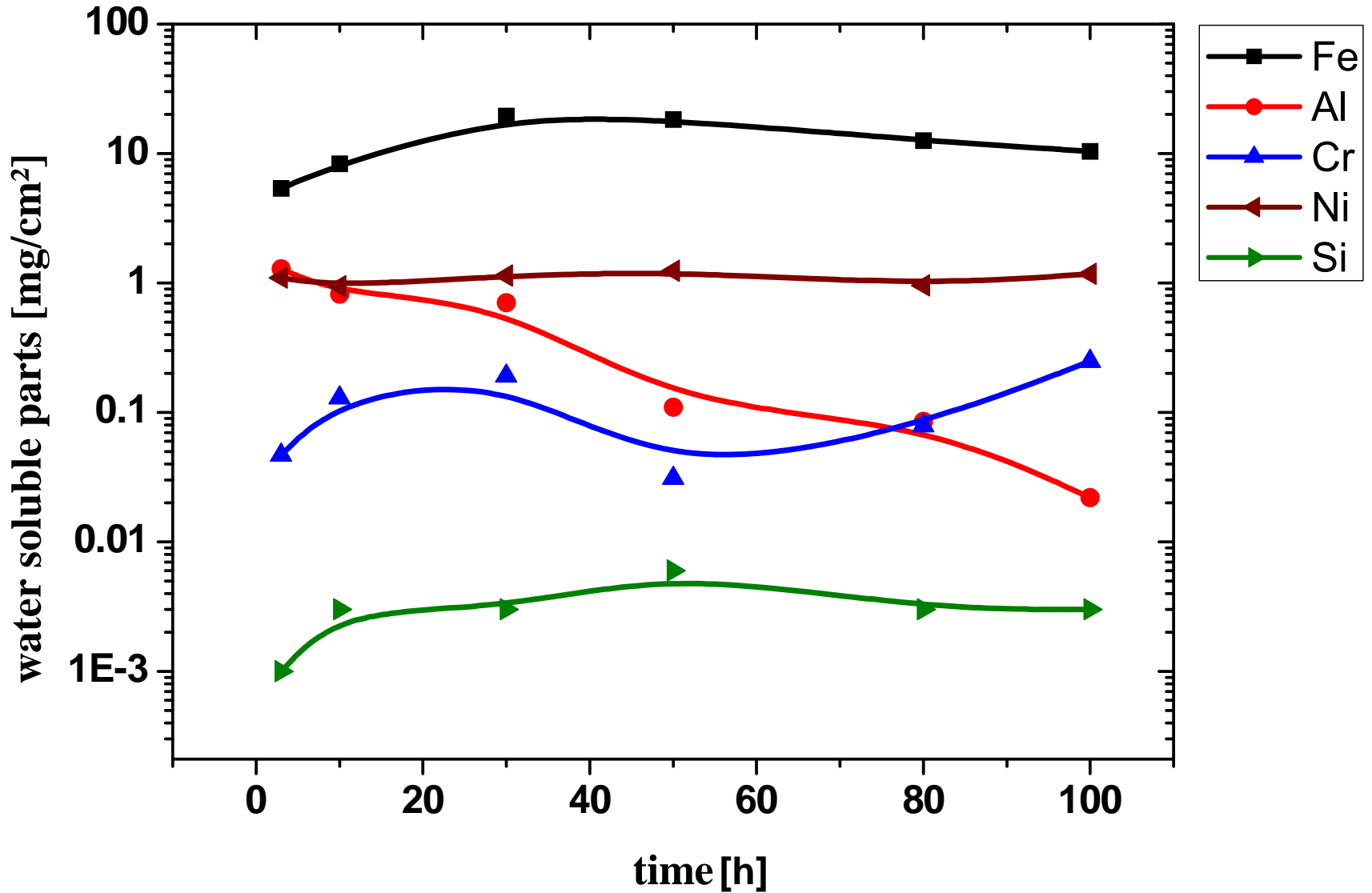


Fe-40Al

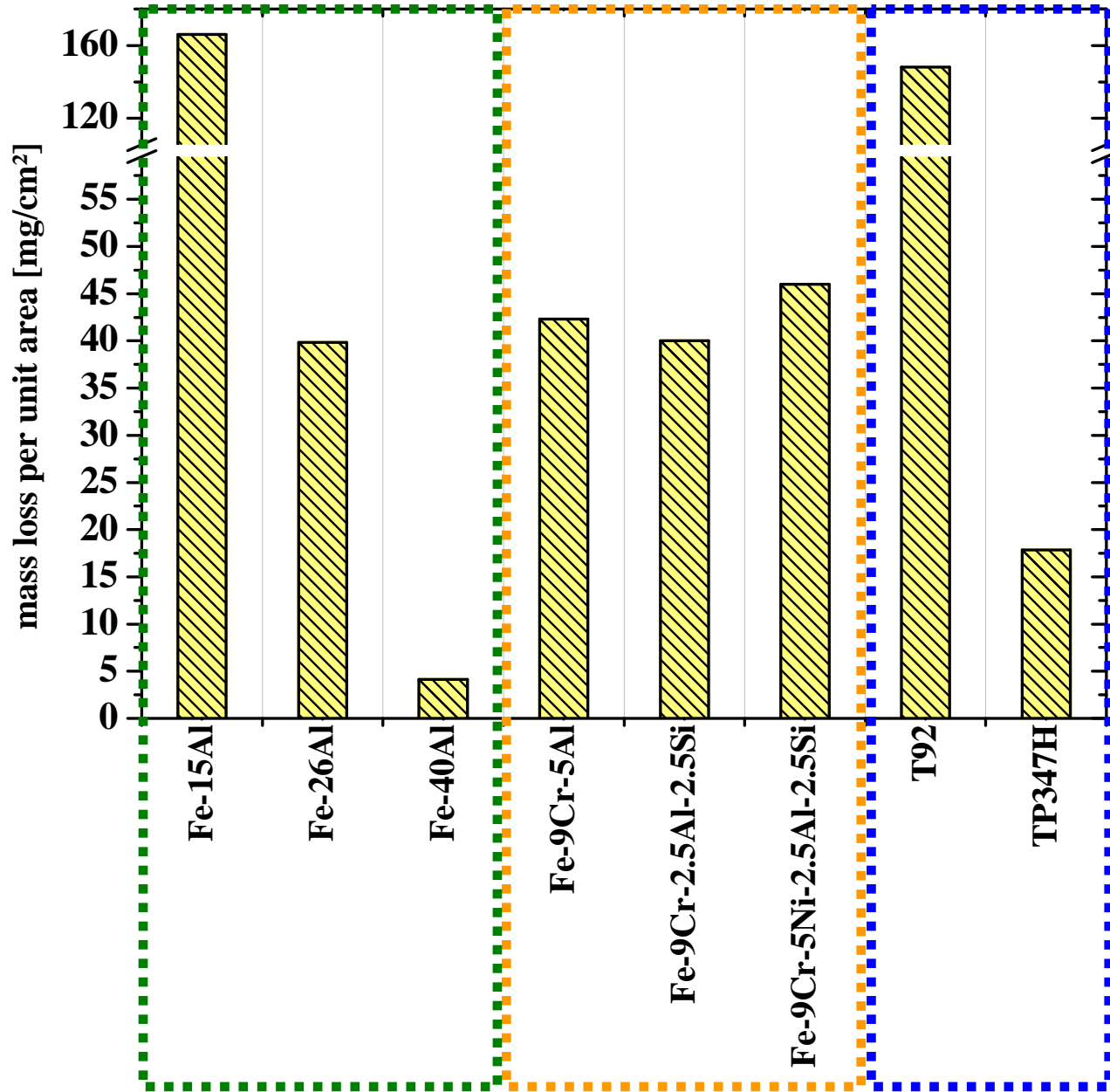








Waste, $(\text{Na}_2\text{-K}_2\text{-Ca-Zn})\text{SO}_4$, 600°C, 336 h



- Commercial steels
 - decrease in mass loss by increasing Cr-/Ni-content
 - strong interaction of Cr and W concerning the degradation mechanism
- Iron aluminides:
 - improved corrosion resistance by increasing the Al-concentration
 - except: KCl-ZnCl₂ -> Fe/Al ratio important for low corrosion
- Modified 9%Cr-steels:
 - beneficial behaviour of Al, Si, Ni concerning 'Active Oxidation'
 - Modifications show no increased corrosion performance at combined degradation mechanisms, i.e. 'Hot Corrosion' and 'Active Oxidation'



Thank you for your attention!